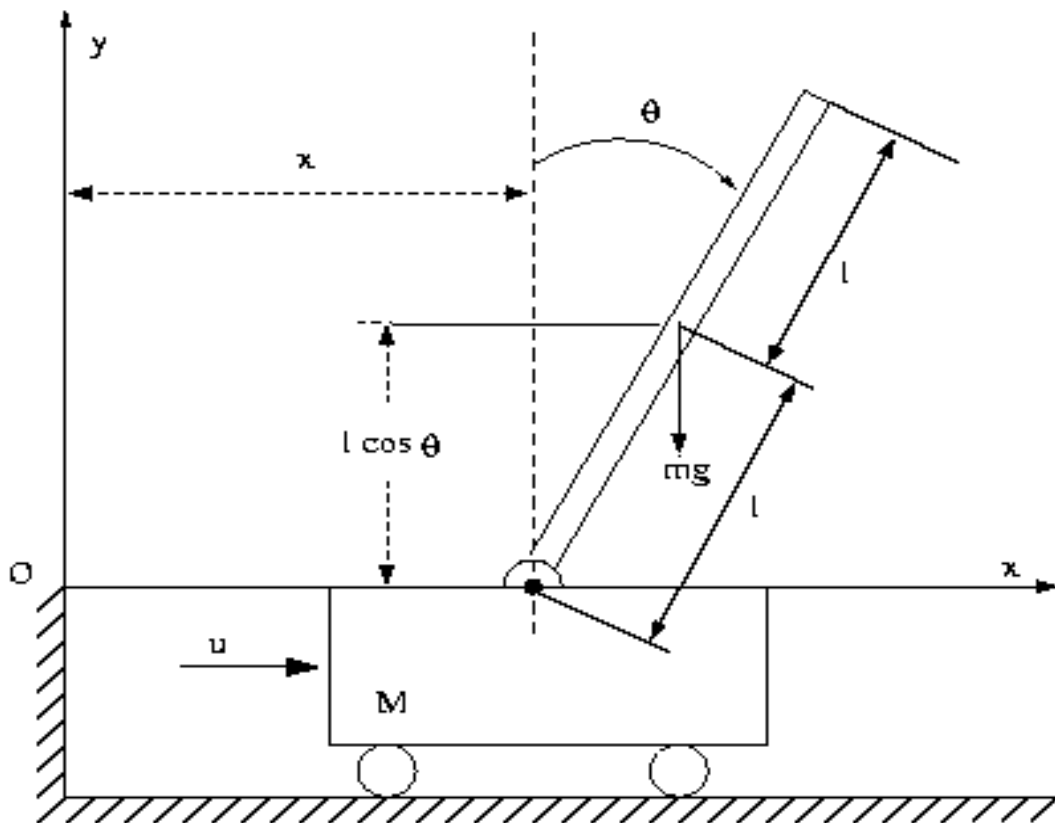


## EE380: Control Systems Laboratory

### Experiment No. 6 Balancing an inverted pendulum

An inverted pendulum mounted on a motor-driven cart is shown in the following figure. This is a model of the attitude control of a space booster on takeoff. (The objective of the attitude control problem is to keep the space booster in a vertical position.) The inverted pendulum is unstable in that it may fall over any time in any direction unless a suitable control force is applied. Here we consider only a two-dimensional problem in which the pendulum moves only in the plane of page. The control force  $u$  is applied to the cart. Assume that the center of gravity of the pendulum rod is at its geometric center.



System Parameters:

Cart Mass  $M = 0.5$  kg

Pendulum Mass  $m = 0.23$  kg

Motor Torque Constant  $K_m = 0.00767$  Nm/A

Motor gear ratio  $K_g = 3.71$

Pendulum length from pivot to the center of gravity  $l = 0.32065$  m

Motor armature resistance  $R = 2.3585 \ \Omega$

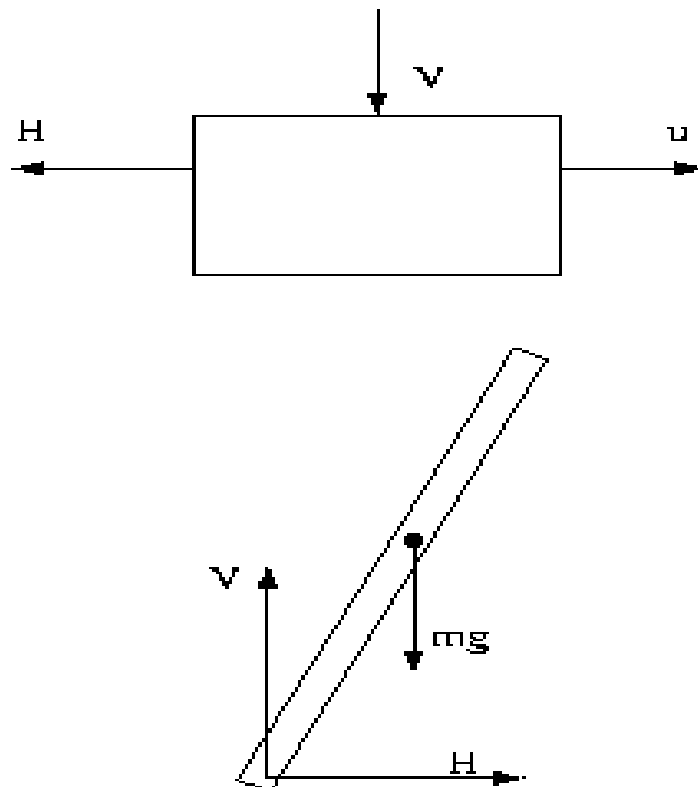
radius of gear connected to motor shaft  $r = 0.00635$  m

### Mathematical Model of the system

Define the angle of the rod from the vertical line as  $\theta$ . Define also the  $(x, y)$  coordinates of the center of gravity of the pendulum rod as  $(x_G, y_G)$ . Then

$$\begin{aligned}x_G &= x + l \sin \theta \\y_G &= l \cos \theta\end{aligned}$$

To derive the equations of motion for the system, consider the free-body diagram shown in the following figure.



The rotational motion of the pendulum rod about its center of gravity can be described by

$$I \ddot{\theta} = V l \sin \theta - H l \cos \theta \quad (1)$$

where  $I$  is the moment of inertia of the rod about its center of gravity. The horizontal motion of center of gravity of pendulum rod is given by

$$m \frac{d^2}{dt^2} (x + l \sin \theta) = H \quad (2)$$

The vertical motion of center of gravity of pendulum rod is

$$m \frac{d^2}{dt^2} (l \cos \theta) = V - mg \quad (3)$$

The horizontal motion of cart is described by

$$M \frac{d^2 x}{dt^2} = u - H \quad (4)$$

Equations (1) – (4) describe the motion of inverted pendulum-on-the cart system. Because these equations involve  $\sin \theta$  and  $\cos \theta$ , they are nonlinear equations.

Since, we are assuming that the mass of the pendulum rod is concentrated at its center of gravity, we take  $I = 0$ . Since our objective is to balance the pole at its top vertical position, we linearize the system around  $\theta = 0$ . For small  $\theta$ ,  $\sin \theta \approx \theta$  and  $\cos \theta \approx 1$ . For small  $\theta$ , we can linearize the equations (1) – (4) as follows:

$$I \ddot{\theta} = V l \theta - H l \quad (5)$$

$$m (\ddot{x} + l \ddot{\theta}) = H \quad (6)$$

$$0 = V - mg \quad (7)$$

$$M \ddot{x} = u - H \quad (8)$$

From equations (6) and (8), we get

$$(M + m) \ddot{x} + m l \ddot{\theta} = u \quad (9)$$

From equations (5) and (7), we get

$$(I + m l^2) \ddot{\theta} + m l \ddot{x} = mgl \theta \quad (10)$$

Equations (9) and (10) may be put in the form of state space model (assuming  $I = 0$ ) as follows:

$$\dot{x} = A x + B u$$

or

$$\begin{bmatrix} \dot{x} \\ \ddot{x} \\ \dot{\theta} \\ \ddot{\theta} \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 & 0 \\ 0 & 0 & \frac{-mg}{M} & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 0 & \frac{(M+m)g}{Ml} & 0 \end{bmatrix} \begin{bmatrix} x \\ \dot{x} \\ \theta \\ \dot{\theta} \end{bmatrix} + \begin{bmatrix} 0 \\ \frac{1}{M} \\ 0 \\ \frac{-1}{Ml} \end{bmatrix} u \quad (11)$$

$u$  is the force applied to the cart in N. It can be expressed in terms of input voltage  $V_i$  as follows:

$$u = \frac{K_m K_g}{Rr} V_i - \frac{K_m^2 K_g^2}{Rr^2} \dot{x} \quad (12)$$

Substituting  $u$  in (11) from (12), we get

$$\begin{bmatrix} \dot{x} \\ \ddot{x} \\ \dot{\theta} \\ \ddot{\theta} \end{bmatrix} = \begin{bmatrix} 0 & 0 & 0 & g \\ \frac{-K_c^{2K} 2}{Rr^{2M}} & \frac{-mg}{M} & 0 & 0 \\ 0 & 0 & 1 & 0 \\ g & \frac{K_c^{2K} 2}{Rr^{2Ml}} & \frac{(M+m)g}{Ml} & 0 \end{bmatrix} \begin{bmatrix} x \\ \dot{x} \\ \theta \\ \dot{\theta} \end{bmatrix} + \begin{bmatrix} 0 \\ \frac{K_m K_g}{MRr} \\ 0 \\ \frac{-K_m K_g}{MlRr} \end{bmatrix} V_i \quad (13)$$

Substituting the values of system parameters, we get state matrix A and input matrix B as follows:

$$A = \begin{bmatrix} 0 & 1 & 0 & 0 \\ 0 & -17.02 & -4.5 & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 53.08 & 44.6 & 0 \end{bmatrix} \quad \text{and} \quad B = \begin{bmatrix} 0 \\ 3.8 \\ 0 \\ -11.85 \end{bmatrix}$$

## Problems

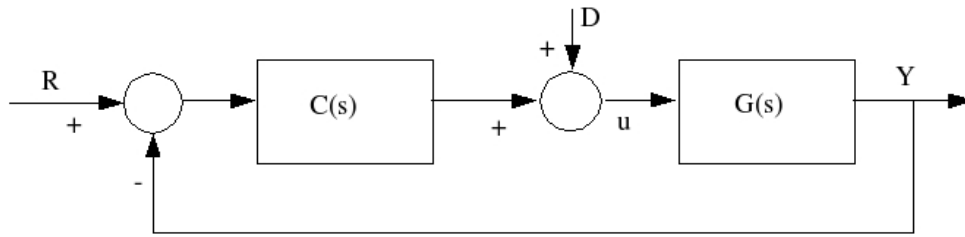
1. Consider the linear model (13). Compute the transfer functions

$$G_1(s) = \frac{\Theta(s)}{V_i(s)} \quad \text{and} \quad G_2(s) = \frac{X(s)}{V_i(s)} \quad \text{where } \theta \text{ and } x \text{ are angular}$$

position of pendulum and linear position of cart respectively.

2. Design a lead compensator to control the angular position  $\theta$  using root locus technique such that the root locus of compensated system passes through dominant poles  $s = -1.5 \pm 1.5i$ .

- Plot the root locus of open loop system.
- Plot the root locus of compensated system.
- Plot the response of the compensated system for a step disturbance at the control input as shown in the following diagram.



3. Find the state feedback gain vector  $K$  such that the control input  $u = -Kx$  stabilizes the system around its equilibrium point and minimizes the following cost function:

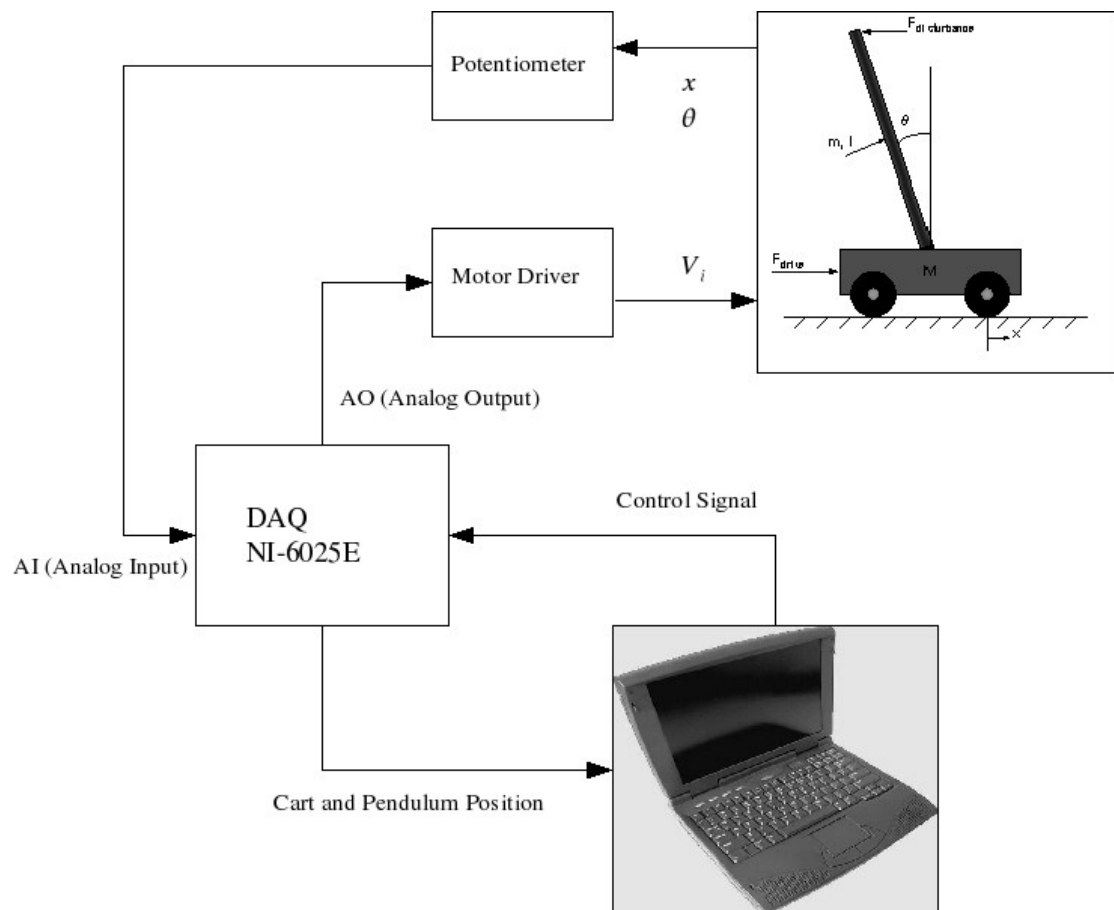
$$J = \int (x' Qx + r V_i^2) dt$$

where

$$Q = \begin{bmatrix} 0.25 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 15 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \quad \text{and} \quad r = 0.0005$$

The resulting closed loop system is termed as linear quadratic regulator (LQR).

- Plot the time response of the closed system for initial condition  $x_0 = [0.2 \ 0 \ 0.2 \ 0]$
  - Also plot the control input.
4. Interface the cart pole system to a personal computer using a data acquisition card as per the block diagram shown below. Implement the LQR controller designed in Problem 3 in real time. Collect real time data for control input, cart position and pole angular position and plot them.



### System Specifications

DC servomotor Rated Voltage : 6V

DC servomotor maximum continuous current: 1 A

Cart Potentiometer sensitivity: 0.0783 m/V

Pole Potentiometer sensitivity: 0.325 rad/V

Potentiometer bias voltage:  $\pm 12$  V

Cart Potentiometer measurement range:  $\pm 5$  V

Following Matlab Commands would be helpful for performing this experiment. Please go through on-line help for more details.

`margin, rlocus, feedback, step, lqr, ss2tf, tf, ode45, plot, function, pole, zero, pzmap.`