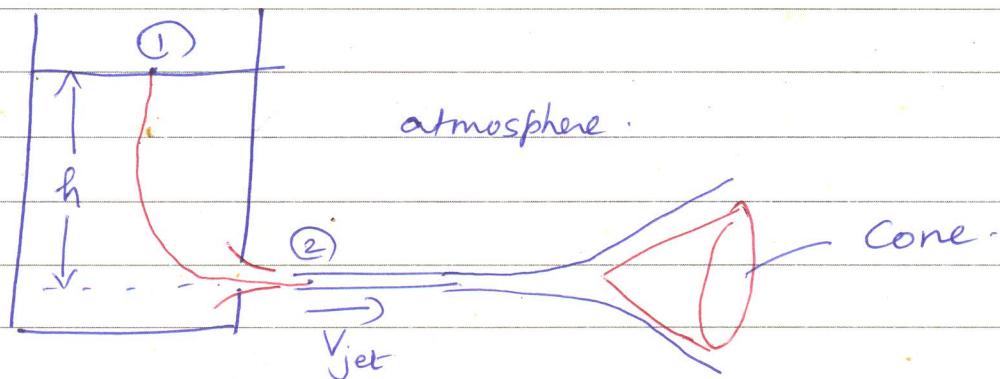


①



(a) To find V_{jet} , apply Bernoulli eqn between points ① & ② which lie on the same streamline.

$$\frac{p_1}{\rho} + g z_1 + \frac{v_1^2}{2} = \frac{p_2}{\rho} + g z_2 + \frac{v_2^2}{2}$$

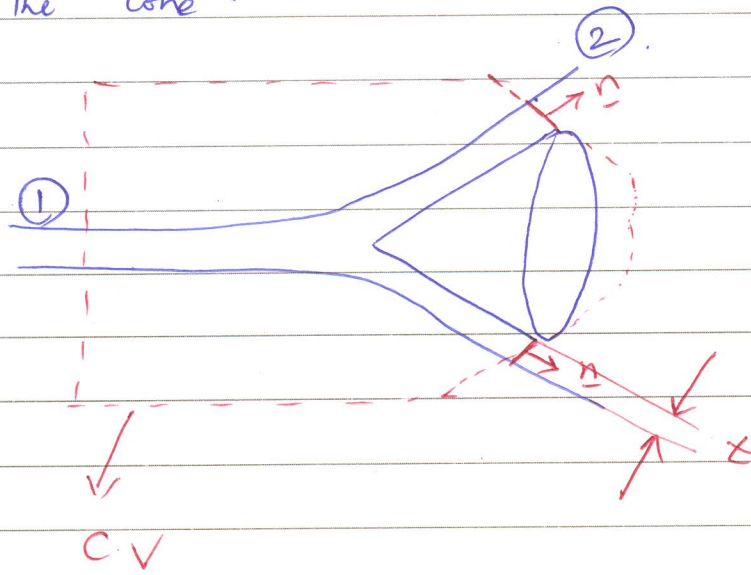
$$p_1 = p_2 = P_{atm}, \quad v_1 \approx 0, \quad (z_1 - z_2) = h.$$

$$\Rightarrow v_2^2 = 2gh \quad \Rightarrow v_2 = \sqrt{2gh}$$

$$v_2 = \sqrt{2 \times 9.8 \times 45.92}$$

$$V_{jet} = v_2 = 30 \text{ m/s.} \quad \text{--- 4 points}$$

(b) It is convenient to be in the ref. frame of the cone.



mass cons. $\Rightarrow -S_1 V_1 A_1 + S_2 V_2 A_2 = 0$

$S_1 = S_2 = S$

$\Rightarrow (V_1 + V_c) \frac{\pi D_1^2}{4} = (V_2 + V_c) \frac{2\pi RL}{4}$

$(30 + 14) \frac{(100 \times 10^{-3})^2}{4} = (V_2 + 14) \frac{2 \times 230 \times 10^{-3} \times 5.434 \times 10^{-3}}{4}$

area over which fluid is leaving normally to the C.S.

$\Rightarrow V_2 = 30 \text{ m/s}$ (w.r.t stationary frame of ref.)

$V_2 = 44 \text{ m/s}$ in the ref. frame of the cone,

4 points



(c) Momentum balance (for the same C.V. shown in page 2)

steady:
x-component

$$F_x = \int_{C.S.} u \rho \underline{v} \cdot \underline{n}$$

$$R_x = u_1 (-\rho V_1 A_1) + u_2 (\rho V_2 A_2)$$

external force on the C.V.

force to be applied on the cone.

in this problem: $V_1 = V_2 = V_j$ $A_2 = A_1 = A_j$
--

$$R_x = - (V_j + V_c) \rho (V_j + V_c) A_j + (V_j + V_c) \cos 60^\circ \rho (V_j + V_c) A_j$$

$$\Rightarrow R_x = \rho (V_j + V_c)^2 A_j [\cos 60^\circ - 1]$$
$$= 10^3 (4)^2 \frac{\pi}{4} (0.1)^2 \left(\frac{1}{2} - 1\right)$$

$$= -7602.65 \text{ N}$$

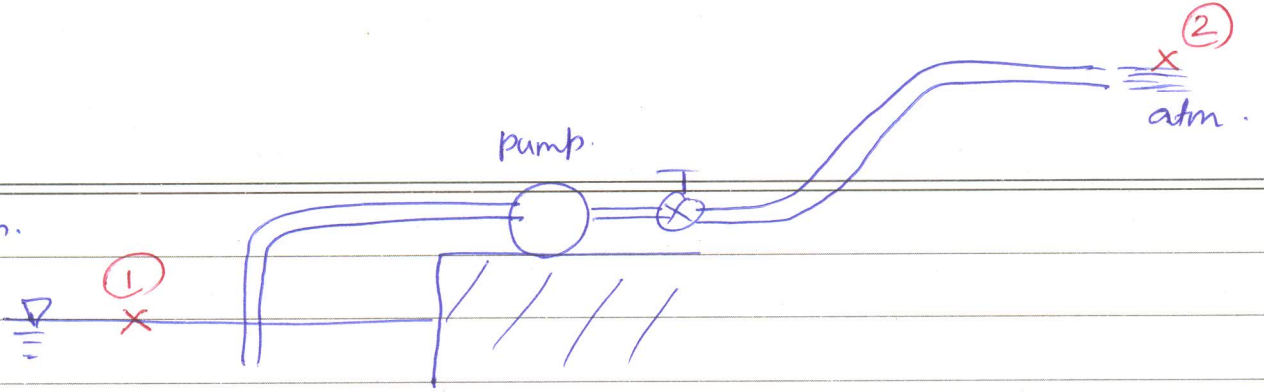
$$= -7.6 \text{ kN}$$

6 points

force in the negative x direction } = 7.6 kN
that must be exerted on the cone

(2)

atm.



- minor losses :
- (1) entrance
 - (2) 90° elbow - 1
 - (3) Gate valve
 - (4) 45° elbow - 2.

Apply energy balance between (1) & (2) :

2 points

$$\left(\frac{p_1}{\rho} + \alpha \frac{\bar{v}_1^2}{2} + g z_1 \right) - \left(\frac{p_2}{\rho} + \alpha_2 \frac{\bar{v}_2^2}{2} + g z_2 \right) + \Delta h_{\text{pump}} = h_{\text{ET}} \begin{cases} h_{\text{major}} \\ h_{\text{minor}} \end{cases}$$

2 points

$$h_{\text{maj}} = f \frac{L}{D} \frac{\bar{v}^2}{2}$$

$$h_{\text{min}} = \frac{\bar{v}^2}{2} \sum_i K_i$$

$$p_1 = p_2 = p_{\text{atm}} \quad \bar{v}_1 = 0 \quad ; \quad \bar{v}_2 = 37 \text{ m/s.} \\ \alpha_2 = 1 \quad (\text{free jet})$$

NOTE : \bar{v}_2 at the nozzle exit is not the avg \bar{v} in the pipe.

If you have used \bar{v}_2 for velocity in the pipe, you will be given half the total grade for if the procedure page 4 is correct.

$$\Rightarrow \Delta h_{\text{pump}} = g z_2 + \frac{\bar{v}_2^2}{2} + f \frac{L}{D} \frac{\bar{v}^2}{2} + \frac{\bar{v}^2}{2} \left[K_{\text{entr}} + K_{90^\circ} + 2 K_{45^\circ} + K_{\text{gate}} \right]$$

in the pipe:

$$\bar{v} = \frac{Q}{A} = \frac{Q}{\frac{\pi D^2}{4}} = 4.84 \text{ m/s.} \quad (2 \text{ points})$$

$$Re = \frac{4.84 \times 100 \times 10^{-3} \times 10^3}{10^{-3}}$$

$$Re = 4.84 \times 10^5$$

$$\epsilon = 0.0015 \text{ mm.}$$

$$\Rightarrow \frac{\epsilon}{D} = 1.5 \times 10^{-5}$$

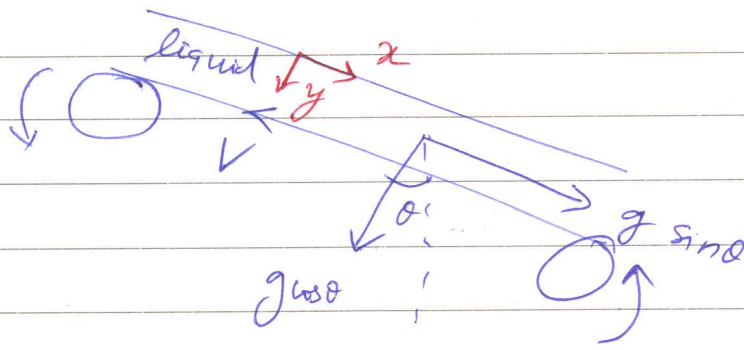
from f - Re chart $\Rightarrow f = 0.0135$. (2 points)

$$\Delta h_{\text{pump}} = 2.249 \times 10^3 \text{ m}^2/\text{s}^2 \quad (2 \text{ points})$$

$$\text{Power i/p} = \dot{m} \Delta h_{\text{pump}} = \frac{10^3 \times 38 \times 2.249 \times 10^3}{10^3}$$

Power i/p to the pump.	= 85.5 kW.	(2 points)
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3.



Boundary conds.

(a) $V_x(y=0) = 0$
 $V_x(y=b) = -V$

2 points

(b)

x-mom: $\mu \frac{d^2 V_x}{dy^2} + \rho g \sin \theta = 0$

$$\frac{d^2 V_x}{dy^2} = -\frac{\rho g \sin \theta}{\mu}$$

$$\frac{dV_x}{dy} = -\frac{\rho g \sin \theta}{\mu} y + C_1$$

$$V_x = -\frac{\rho g \sin \theta}{\mu} \frac{y^2}{2} + C_1 y + C_2$$

use BC's $\Rightarrow C_1 = \frac{\rho g \sin \theta}{2\mu} b - \frac{V}{b}$; $C_2 = 0$

$$V_x(y) = \frac{\rho g \sin \theta b^2}{2\mu} \left[\frac{y}{b} - \frac{y^2}{b^2} \right] - \frac{V}{b} y$$

$$Q \text{ (per unit width)} = \int_0^b v_x dy$$

$$Q = \frac{\rho g \sin \theta b^3}{12 \mu} - \frac{v b}{2} \quad \boxed{2 \text{ points}}$$

$$\text{If } Q = 0 \quad v_c = \frac{\rho g \sin \theta b^2}{6 \mu}$$

$$= \frac{10^3 \times 9.8 \times \frac{1}{\sqrt{2}} \times (0.01)^2}{6 \times 0.1}$$

$$\Rightarrow \boxed{v_c = 1.155 \text{ m/s}} \quad \boxed{2 \text{ points}} \quad |$$

4 (a). Euler eqn: (steady)

$$\rho (\underline{v} \cdot \nabla) \underline{v} = -\nabla p + \rho \underline{g}$$

vector identity: $(\underline{v} \cdot \nabla) \underline{v} = \nabla \left(\frac{1}{2} \underline{v} \cdot \underline{v} \right) + \underbrace{(\nabla \times \underline{v}) \times \underline{v}}_{\underline{\omega}}$

$$\Rightarrow \left[\nabla \left(\frac{1}{2} \underline{v} \cdot \underline{v} \right) + \underline{\omega} \times \underline{v} + \frac{1}{\rho} \nabla p - \underline{g} \right] \cdot d\underline{r} = 0$$

along a streamline, $(\underline{\omega} \times \underline{v}) \cdot d\underline{r} = 0$
 $\underline{g} = -g \hat{k}$

$$\Rightarrow \nabla \left(\frac{1}{2} \underline{v} \cdot \underline{v} \right) \cdot d\underline{r} + \frac{1}{\rho} \nabla p \cdot d\underline{r} - \underline{g} \cdot d\underline{r} = 0$$

$$\Rightarrow d \left(\frac{1}{2} \underline{v} \cdot \underline{v} \right) + d \left(\frac{p}{\rho} \right) + g dz = 0$$

\Rightarrow along a streamline

$$d \left[\frac{1}{2} v^2 + \frac{p}{\rho} + gz \right] = 0$$

$$\Rightarrow \left(\frac{v^2}{2} + \frac{p}{\rho} + gz \right) = \text{Const. along a streamline.}$$

4 (b) Streamlines \Rightarrow const $\psi \Rightarrow d\psi = 0$.

$$d\psi = \frac{\partial\psi}{\partial x} dx + \frac{\partial\psi}{\partial y} dy = 0.$$

$$\text{slope of a streamline} \Rightarrow \left. \frac{dy}{dx} \right|_{\psi} = \frac{-\partial\psi/\partial x}{\partial\psi/\partial y} = \frac{v}{u}.$$

equipotential \Rightarrow const $\phi \Rightarrow d\phi = 0$.

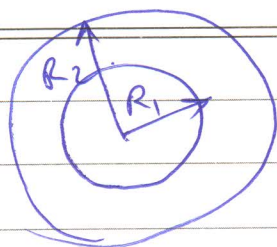
$$d\phi = u dx + v dy = 0.$$

$$\left. \frac{dy}{dx} \right|_{\phi} = -\frac{u}{v}.$$

multiplying the two slopes \Rightarrow

7 $\frac{v}{u} \times \left(-\frac{u}{v}\right) = -1 \Rightarrow$ Streamlines & equipotentials are orthogonal.

5 a).



$$\frac{d}{dr} \left(r^2 \frac{dT}{dr} \right) = 0$$

$$\frac{dT}{dr} = \frac{C_1}{r^2} \Rightarrow T_1 = -\frac{C_1}{r} + C_2$$

$$T = T_1 \quad \text{at } r = R_1$$

$$T = T_2 \quad \text{at } r = R_2$$

↪ unknown yet.

$$C_1 = \frac{T_1 - T_2}{\left(\frac{1}{R_2} - \frac{1}{R_1}\right)} ; \quad C_2 = \frac{-T_2 + T_1 \frac{R_1}{R_2}}{R_1 \left(\frac{1}{R_2} - \frac{1}{R_1}\right)}$$

$$T = T_1 + \frac{T_2 - T_1}{\frac{1}{R_1} - \frac{1}{R_2}} \left(\frac{1}{R_1} - \frac{1}{r} \right)$$

$$Q_{th} = - (4\pi r^2) k \frac{dT}{dr} = \frac{4\pi k (T_1 - T_2)}{\left(\frac{1}{R_1} - \frac{1}{R_2}\right)}$$

$$R_{th, cond} = \frac{1}{4\pi k} \left(\frac{1}{R_1} - \frac{1}{R_2} \right) \text{ --- (3) points}$$

$$R_{th, conv} = \frac{1}{4\pi R_2^2 h} \text{ --- (1) point}$$

$$\frac{d R_{tot}}{d R_2} = 0 \Rightarrow \boxed{R_{2c} = \frac{2k}{h}} \text{ (3) points}$$

5 (b) $Bi = \frac{hR}{k} = \frac{1 \times 0.5 \times 10^{-3}}{1} = 5 \times 10^{-4} \ll 1$

\Rightarrow Tempr. variation in the body negligible. (2)

$$\theta^* = \frac{T - T_f}{T_0 - T_f} = \exp \left[\underbrace{\frac{-hA}{SVC}}_{} t \right]$$

$$T_0 = 30^\circ$$

$$T_f = 100^\circ$$

$$T = 80^\circ \text{ --- (2) points}$$

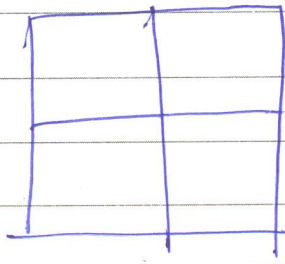
$\Rightarrow \frac{2}{7} = \exp \left[\frac{-2\pi R L \cdot 1}{8\pi R^2 L \cdot C} t \right]$ (1) point

$$= \exp \left[\frac{-2}{\cancel{2} \cdot 10^3 \cdot \frac{1}{2} \cdot 10^3 \cdot \cancel{4} \cdot 10^3} t \right]$$

$\Rightarrow \frac{2}{7} = \exp \left[-\frac{1}{2000} t \right]$

$t \approx 42 \text{ mins.}$ (2) points

$$6(a) \quad C_f = \frac{C_1}{\sqrt{Re_L}} \quad \underline{1}$$



$$F_A = \frac{C_1}{\sqrt{2L_1}} \cdot 4A_1 \sqrt{\frac{v_s}{\mu}}$$

$$F_B = \frac{C_1}{\sqrt{4L_1}} \cdot 1 \cdot 4A_1 \sqrt{\frac{v_s}{\mu}}$$

$$\Rightarrow F_A = \sqrt{8} F_1$$

$$F_B = 2 F_1$$

(T)

$$\Rightarrow F_A > F_B$$

6(b) density of naphthalene at the surface : = S_{A0} .

$$pV = \frac{m}{M} RT$$

$$S_{A0} = \frac{m}{V} = \frac{p_A M}{RT} = \frac{\left(\frac{1}{760} \times 1.013 \times 10^5 \text{ Pa}\right) 128}{8314 \cdot 300}$$

$$S_{A0} = 6.8 \times 10^{-3} \text{ kg/m}^3 \quad \underline{2}$$

$$\frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial S_A}{\partial r} \right) = 0$$

$$S_A = \frac{C_1}{r} + C_2$$

$$S_A (r=R_1) = S_{A0}$$

$$S_A (r \rightarrow \infty) = 0$$

$$\Rightarrow S_A = \frac{S_{A0}}{r} R_1$$

$$\text{flux} = -D_{AB} \left. \frac{\partial S_A}{\partial r} \right|_{r=R_1} = D_{AB} \frac{S_{A0}}{R_1^2}$$

$$\begin{aligned} \text{Rate of evap.} &= \text{flux} \cdot 4\pi R_1^2 \\ &= 4\pi R_1 D_{AB} S_{A0} \end{aligned}$$

$$= 4\pi \left(\frac{1}{2} \times 10^{-2} \right) \times \left(5 \times 10^{-6} \right) \times \left(6.8 \times 10^{-3} \right)$$

$$= 2.136 \times 10^{-9} \text{ kg/s} \quad 5$$

(7)