Introduction to Hydrodynamic Stability

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SADEAFFP-2014, Department of Mathematics, IIT Kanpur

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Hydrodynamic Stability

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Outline



- 2 Linear stability theory
- 3 A toy example
- 4 Kelvin-Helmholtz instability
- 5 Capillary Instability
- 6 Parallel shear flows

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References

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- Water flow from a tap.
- Smoke from an incence stick.
- Flow between two concentric cylinders.
- A layer of heated liquid.



Fig. 63 Watan dial .

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Hydrodynamic stability: connection with Mathematics

- Pioneers: Applied Mathematicians and Mathematical Physicists in late 1800s and early 1900s.
- E.g. von Helmholtz, Lord Kelvin, Lord Rayleigh, Neils Bohr, A Sommerfeld, W Heisenberg (PhD thesis, 1923), S Chandrasekhar, V I Arnold...
- One of the 7 Millennium Prize problems of Clay Mathematical Institute.

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Navier-Stokes Equation

Waves follow our boat as we meander across the lake, and turbulent air currents follow our flight in a modern jet. Mathematicians and physicists believe that an explanation for and the prediction of both the breeze and the turbulence can be found through an understanding of solutions to the Navier-Stokes equations. Although these equations were written down in the 19th Century, our understanding of them remains minimal. The challenge is to make substantial progress toward a mathematical theory which will unlock the secrets hidden in the Navier-Stokes equations.

Laminar-turbulent transition

• Osborne Reynolds (1883), "An experimental investigation of the circumstances which determine whether the motion of water shall be direct or sinuous.."



• Discontinuous transition from laminar to a turbulent flow when $Re \equiv \rho VD/\mu > 2000.$

• For rectangular channels, transition at $Re \sim 1200$.

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- Newtonian fluids: Navier-Stokes equations have all the information about fluid flow.
- Laminar flows: simple solutions to governing equations.
- Examples: plane and pipe Poiseuille flows; plane Couette flow.
- Flow in a pipe: laminar flow unstable at $Re \sim 2000$.
- Instability leads to *turbulence*.
- Turbulent flows: high mixing and drag.
- Laminar flows: low mixing and drag.
- When does a given laminar flow become unstable ?

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Navier-Stokes equations

$$\nabla \cdot \mathbf{v} = 0$$
 $Re[\partial_t \mathbf{v} + \mathbf{v} \cdot \nabla \mathbf{v}] = -\nabla p + \nabla^2 \mathbf{v}$

- Laminar flows: flows with relatively simple kinematics and are usually time-independent.
- Laminar flow solutions satisfy Navier-Stokes equations at any Re.

Landau & Lifshitz

"Yet not every solution of the equations of motion, even if it is exact, can actually occur in Nature. The flows that occur in Nature must not only obey the equations of fluid dynamics, but also be stable"

• Need to probe the stability of laminar flows to external disturbances.

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Need to probe the stability of laminar flows to external disturbances.

- Real flows subjected to disturbances of various types.
- Disturbances distort the existing force equilibrium.
- Thermal convection & Circular Couette flows.

After instability

- New complex laminar states.
- Direct transition to turbulence.

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• Experiments, computation and theory.

- What is the effect of an initial disturbance on laminar flow ?
- Do perturbations grow or decay ?
- At what value of Reynolds number ?
- Infinitesimal vs. finite disturbances.
- Infinitesimal disturbances: unavoidable.
- Linear stability theory.

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Specify governing equations

Navier-Stokes equations (Newtonian fluid)

$$abla \cdot {f v} = {f 0}\,,$$

$$\rho[\partial_t \mathbf{v} + (\mathbf{v} \cdot \nabla)\mathbf{v}] = -\nabla \rho + \mu \nabla^2 \mathbf{v} + \rho \mathbf{g}.$$

Boundary conditions at rigid surface: no-slip and no-penetration.

Find the base state: $\overline{v}_x(z)$, and $\overline{p}(x)$ (steady, unidirectional).

Specify appropriate constitutive relation.

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For complex fluids

Specify appropriate constitutive relation.

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Add a small perturbation

$$\mathbf{v}(\mathbf{x},t) = \overline{\mathbf{v}}_{\mathbf{x}}(\mathbf{x}) + \delta \mathbf{v}'(\mathbf{x},t), \quad p(\mathbf{x},t) = \overline{p}(\mathbf{x}) + \delta p'(\mathbf{x},t), \quad |\delta| \ll 1.$$



Key questions

- For a given control parameter λ, does v' grow or decay with time ?
- What is the critical λ for instability ?
- What is the spatial structure at the critical value ?

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Nonlinear term in Navier-Stokes:

$$\mathbf{v} \cdot \nabla \mathbf{v} = \overline{\mathbf{v}} \cdot \nabla \overline{\mathbf{v}} + \delta(\overline{\mathbf{v}} \cdot \nabla \mathbf{v}' + \mathbf{v}' \cdot \nabla \overline{\mathbf{v}}) + \delta^2 \mathbf{v}' \cdot \nabla \mathbf{v}'$$

v • v v is the trivial laminar-flow contribution.

- At $O(\delta)$, terms linear in the perturbations \Rightarrow Include.
- At O(δ²), terms non-linear in the perturbations ⇒ Neglected for small perturbations.
- Hence, *linear* stability.
- Can predict only the *onset* of instability.

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Linearized PDEs: Fourier expansion

Collect terms of $O(\delta)$:

$$abla \cdot \mathbf{v}' = \mathbf{0}$$

$$\rho[\partial_t \mathbf{v}' + \overline{\mathbf{v}} \cdot \nabla \mathbf{v}' + \mathbf{v}' \cdot \nabla \overline{\mathbf{v}}] = -\nabla p' + \mu \nabla^2 \mathbf{v}'$$

BCs: $\mathbf{v}' = 0$ at rigid boundaries; Initial condition $\mathbf{v}'(\mathbf{x}, t = 0)$. MEAN FLOW: $(V_x(y), \theta, \theta)$

Fourier expand the disturbances

$$A(\mathbf{x},t) = \int_{-\infty}^{+\infty} dk_x \int_{-\infty}^{+\infty} dk_z \sum_{n=1}^{\infty} A_n(k,t) F_n(y) \exp[i(k_x x + k_z z)]$$

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● Linearity ⇒ Study the dynamics of all Fourier modes *individually*.

- Time dependence $A_n(k, t) = A_n(k) \exp[s_n t]$
- Complex growth rate $s = s_r + is_i$
- $s_r > 0$ Instability; $s_r < 0$ Stability; $s_r = 0$ Neutral stability.
- If any Fourier mode grows with time \Rightarrow unstable, exponential growth as $t \rightarrow \infty$.
- If all Fourier modes decay \Rightarrow stable as $t \rightarrow \infty$.
- Need to solve coupled ODEs (for F(y)) with an eigenvalue s for various values of control parameter λ.

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- Governing equation: $\partial_t f = f f^2 + \frac{1}{\lambda} \partial_y^2 f$
- Boundary conditions: f(y = 0) = f(y = 1) = 0.
- Base state: $\overline{f} = 0$
- Add perturbation: $f(y,t) = \overline{f} + \delta f'(y,t)$
- Linearize: $\partial_t(\bar{f} + \delta f') = \bar{f} - \bar{f}^2 + \frac{1}{\lambda} \partial_y^2 \bar{f} + \delta \left[f' - 2\bar{f}f' + \frac{1}{\lambda} \partial_y^2 f' \right] + O(\delta^2) \cdots$
- At $O(\delta)$: $\partial_t f' = f' 2\bar{f}f' + \frac{1}{\lambda}\partial_y^2 f'$
- $\partial_t f' = f' + \frac{1}{\lambda} \partial_y^2 f'$, f'(y = 0) = f'(y = 1) = 0
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- Neutral s = 0 for $\lambda = n^2 \pi^2$
- Unstable s > 0 for $\lambda > n^2 \pi^2$
- Most unstable mode:

•
$$f'(y, t) =$$

 $c \sin[\pi y] \exp\left[\left(1 - \frac{\pi^2}{\lambda}\right) t\right]$

3

•
$$F(y) = c \sin[n\pi y]$$
 n integer.

- $s_n = 1 \frac{n^2 \pi^2}{\lambda}$
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Kelvin-Helmholtz instability - I

- Two incompressible, inviscid fluids in horizontal parallel infinte streams of different densities and velocities, one stream above the other.
- $\mathbf{U}(z) = U_2 \mathbf{i}, \ \rho(z) = \rho_2, \ P(z) = \rho_0 g \rho_2 z \text{ for } z > 0.$
- $\mathbf{U}(z) = U_1 \mathbf{i}, \ \rho(z) = \rho_1, \ P(z) = p_0 g \rho_1 z \text{ for } z < 0.$
- Irrotational perturbations: restrictive, but enough for a proof of instability.
- Does not prove stability as the analysis gives no information about rotational disturbances.
- Perturbed interface $z = \zeta(x, y, t)$.
- $\mathbf{u} = \nabla \phi$ where $\phi = \phi_1$ for $z > \zeta$, and $\phi = \phi_2$ for $z < \zeta$.

Kelvin-Helmholtz instability - II

•
$$\nabla \cdot \mathbf{u} = 0$$
, $\nabla \times \mathbf{u} = 0 \Rightarrow \mathbf{u} = \nabla \phi$.

•
$$\nabla^2 \phi_1 = 0$$
 for $z > \zeta$ and $\nabla^2 \phi_2 = 0$ for $z < \zeta$.

• BC:
$$\nabla \phi = \mathbf{U}$$
 as $z = \pm \infty$.

- Kinematic condition at moving interface $z = \zeta$, k = 1, 2: $\frac{D\zeta}{Dt} = u_z^k = \frac{\partial \zeta}{\partial t} + \frac{\partial \phi_k}{\partial x} \frac{\partial \zeta}{\partial x} + \frac{\partial \phi_k}{\partial y} \frac{\partial \zeta}{\partial y}$
- Normal stress continuity (Bernoulli theorem) at $z = \zeta$: $\rho_1 \left[C_1 - \frac{1}{2} (\nabla \phi_1)^2 - \frac{\partial \phi_1}{\partial t} - gz \right] = \rho_2 \left[C_2 - \frac{1}{2} (\nabla \phi_2)^2 - \frac{\partial \phi_2}{\partial t} - gz \right]$
- The base flow also satisfies this condition (at z = 0): $\rho_1 \left(C_1 - \frac{1}{2}U_1^2\right) = \rho_2 \left(C_2 - \frac{1}{2}U_2^2\right)$

Kelvin-Helmholtz instability - Linearization

• $\phi_2 = U_2 x + \phi'_2$ for $z > \zeta$, $\phi_1 = U_1 x + \phi'_1$ for $z < \zeta$. Neglect products of small perturbations ϕ'_1 , ϕ'_2 and ζ . • How small ? $\frac{\partial \zeta}{\partial x}, \frac{\partial \zeta}{\partial y} \ll 1$ and $g\zeta \ll U_1^2, U_2^2$. • Taylor-expand $z = \zeta$ about z = 0: $\phi'_{k}|_{z=\zeta} = \phi'_{k}|_{z=0} + \zeta \frac{\partial \phi'_{k}}{\partial z}|_{z=0} + \cdots$ • $\nabla^2 \phi_2 = 0$. $\nabla^2 \phi_1 = 0$ BC: $\nabla \phi'_{\mu} \rightarrow 0$ for $z \rightarrow \mp \infty$ for k = 1, 2 $\frac{\partial \phi'_k}{\partial z} = \frac{\partial \zeta}{\partial t} + U_k \frac{\partial \zeta}{\partial x}$ at z = 0 for k = 1, 2. $\rho_1\left(U_1\frac{\partial\phi_1'}{\partial x}+\frac{\partial\phi_1'}{\partial t}+g\zeta\right)=\rho_2\left(U_2\frac{\partial\phi_2'}{\partial x}+\frac{\partial\phi_2'}{\partial t}+g\zeta\right) \text{ at } z=0.$

Kelvin-Helmholtz instability - Normal Modes

•
$$(\zeta, \phi'_1, \phi'_2) = (\tilde{\zeta}, \tilde{\phi}_1, \tilde{\phi}_2) \exp[i(kx + ly) + st]$$

• $\nabla^2 \phi'_k \Rightarrow \left[\frac{d^2 \tilde{\phi}_k}{dz^2} - (k^2 + l^2) \tilde{\phi}_k \right] = 0$
• $\tilde{\phi}_2 = A_2 \exp[-\tilde{k}z] + B_2 \exp[\tilde{k}z], \ \tilde{k}^2 = (k^2 + l^2).$
• BC at $y \to \infty, u_z^2 = 0 \Rightarrow B_2 = 0.$
• So: $\tilde{\phi}_2 = A_2 \exp[-\tilde{k}]z$ and $\tilde{\phi}_1 = A_1 \exp[\tilde{k}z].$
• Using the kinematic condition at interface:
 $A_2 = -(s + ikU_2)\tilde{\zeta}/\tilde{k}, \quad A_1 = (s + ikU_1)\tilde{\zeta}/\tilde{k}.$
• Using the normal stress condition at interface:

 $\rho_1[\tilde{k}g + (s + ikU_1)^2] = \rho_2[\tilde{k}g - (s + ikU_2)^2]$

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Kelvin-Helmholtz instability - Growth Rate

•
$$s = -ik \frac{\rho_1 U_1 + \rho_2 U_2}{\rho_1 + \rho_2} \pm \left[\frac{k^2 \rho_1 \rho_2 (U_1 - U_2)^2}{(\rho_1 + \rho_2)^2} - \frac{\tilde{k}g(\rho_1 - \rho_2)}{\rho_1 + \rho_2} \right]^{1/2}$$

- Both roots are neutrally stable if $\tilde{k}g(\rho_1^2 \rho_2^2) \ge k^2 \rho_1 \rho_2 (U_1 U_2)^2$. When the equality holds, marginal stability.
- One root is unstable (with Re[s] > 0) if $\tilde{k}g(\rho_1^2 \rho_2^2) < k^2 \rho_1 \rho_2 (U_1 U_2)^2$.

Surface Gravity Waves

- $\rho_2 = 0$ and $U_1 = 0, U_2 = 0$. Surface gravity waves on deep water.
- Stable with phase velocity: $c = \mathrm{i}s/\tilde{k} = \pm (g/\tilde{k})^{1/2}$
- Oscillatory, stable normal modes.
- Waves a special case of hydrodynamic stability.

Internal Gravity Waves

- No basic flow: $U_1 = 0, U_2 = 0.$
- $s = \pm [\tilde{k}g(\rho_2 \rho_1)/(\rho_1 + \rho_2)^2]^{1/2}$
- Instability if $\rho_1 < \rho_2$ (heavey fluid rests above light fluid).
- If $\rho_1 > \rho_2$, there is stability, and there are waves with phase velocity: $c = \pm [g(\rho_1 - \rho_2)/\tilde{k}(\rho_1 + \rho_2)]^{1/2}$.
- The eigenfunctions decay exponentially away from the interface. Motion confined to the vicinity of the interface.
- Observed between layers of fresh and salt water that occur in estuaries.
- Rayleigh-Taylor instability when the whole system has an upward acceleration f. Same result with g' = f + g. If $\rho_2 > \rho_1$, then instability occurs only of g' < 0.

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Instability Due to Shear

• No effect of buoyancy: $\rho_1 = \rho_2$, but $U_1 \neq U_2$.

•
$$s = -\frac{1}{2}ik(U_1 + U_2) \pm \frac{1}{2}k(U_1 - U_2)$$

Flow always unstable if U₁ ≠ U₂. Waves of all wavelengths are unstable.



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Capillary Instability of a Jet

- A cylindrical jet of liquid moving with *uniform* velocity in air (e.g. water jet from a slightly-open tap).
- Surface tension at the liquid-air interface.
- Assume density of outside fluid is zero, and inviscid dynamics for the liquid.

•
$$\rho\left(\frac{\partial \mathbf{u}}{\partial t} + \mathbf{u} \cdot \nabla \mathbf{u}\right) = -\nabla \rho$$
 $\nabla \cdot \mathbf{u} = 0$
Pressure inside the jet: $P = P_{\infty} + \gamma \nabla \cdot \mathbf{n}$ at $r = \zeta(x, \theta, t)$

• Perturbed unit normal to the jet:

$$\mathbf{n} = \frac{\left(-\frac{\partial \zeta}{\partial x}, 1, -\frac{\partial \zeta}{\partial r\theta}\right)}{\left[\left(\frac{\partial \zeta}{\partial x}\right)^2 + 1 + \left(\frac{\partial \zeta}{\partial r\theta}\right)^2\right]^{1/2}}$$

Capillary Instability of a Jet

- Kinematic condition: $u_r = \frac{D\zeta}{Dt}$ at $r = \zeta$.
- Base flow: $\mathbf{U} = 0$, $P = p_{\infty} + \gamma/a$ for $0 \le r \le a$, as $\nabla \cdot \mathbf{n} = 1/r$ when $\mathbf{n} = \mathbf{e}_r$.
- Disturbances: $\mathbf{u} = \mathbf{U} + \mathbf{u}'$, p = P + p', and $\zeta = a + \zeta'$
- $\rho \frac{\partial \mathbf{u}'}{\partial t} = -\nabla p'$ and $\nabla \cdot \mathbf{u}' = 0.$ • $\nabla \cdot \mathbf{n} = \frac{1}{r} - \frac{\partial^2 \zeta'}{\partial x^2} - \frac{1}{r^2} \frac{\partial^2 \zeta'}{\partial \theta^2}$ • Normal stress BC at r = a: $p' = -\gamma \left(\frac{\zeta'}{a^2} + \frac{\partial^2 \zeta'}{\partial x^2} + \frac{1}{a^2} \frac{\zeta'}{\theta^2} \right)$ • $\nabla^2 p' = 0$, where $\nabla^2 = \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial r^2} + \frac{1}{r} \frac{\partial}{\partial r} + \frac{1}{r^2} \frac{\partial^2}{\partial \theta^2}.$
- Normal modes: $(\mathbf{u}', p', \zeta') = (\tilde{\mathbf{u}}(r), \tilde{\rho}(r), \tilde{\zeta}) \exp[st + i(kx + n\theta)]$

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Capillary Instability of a Jet

•
$$\frac{\mathrm{d}^2 \tilde{p}}{\mathrm{d}r^2} + \frac{1}{r} \frac{\mathrm{d}\tilde{p}}{\mathrm{d}r} - \left(k^2 + \frac{n^2}{r^2}\right) \tilde{p} = 0$$

- Linearly independent solutions: modified Bessel functions $I_n(kr)$, $K_n(kr)$; take $n \ge 0$ without loss of generality.
- Physically allowed solution: $\tilde{p}(r) = AI_n(kr)$.
- $\tilde{\mathbf{u}} = -A(\rho s)^{-1}(ikI_n(kr), kI'_n(kr), inr^{-1}I_n(kr))$
- Linearized BCs: $AI_n(\alpha) = -\gamma(1 \alpha^2 n^2)\tilde{\zeta}/a^2$, $-A(a\rho s)^{-1}\alpha I'_n(\alpha) = s\tilde{\zeta}$ where $\alpha = ak$.
- Eigenvalue relation:

•
$$s^2 = \frac{\gamma}{a^3\rho} \frac{\alpha I'_n(\alpha)}{I_n(\alpha)} (1 - \alpha^2 - n^2)$$

- $\alpha I'_n(\alpha)/I_n(\alpha) > 0$ for all $\alpha \neq 0$. So $s^2 < 0$ if $n \neq 0$.
- $s^2 > 0$ for $-1 < \alpha < 1$ if n = 0.

Dispersion relation: theory and experiments



- Jet stable to all nonaxisymmetric disturbances $(n \neq 0)$.
- Jet unstable to axisymmetric modes with wavelengths $\lambda = 2\pi/k > 2\pi a$.
- If k_m is the wavenumber at which s is maximum, $k_m = 0.7/a$.
- Jets of all radii are unstable. *No critical parameter that marks the domain of stability.*
- In experiments the liquid jet will break up with wavelength about $2\pi/k_m \approx 9a$

Physical interpretation

- Displacement of the jet radius: $R_{new} = R + \epsilon \cos(kz)$, $k = 2\pi/\lambda$.
- Surface area of the perturbed jet:

$$A = \int_{0}^{\lambda} 2\pi R_{new} \, ds$$
$$V = \int_{0}^{\lambda} \pi R_{new}^{2} \, dz$$
$$ds = \left[\left(\frac{\mathrm{d}R_{new}}{\mathrm{d}z} \right)^{2} + 1 \right]^{1/2} \, dz$$
For small ϵ , $ds = \left[1 + \frac{1}{2} \left(\frac{\mathrm{d}R_{new}}{\mathrm{d}z} \right)^{2} \right] \, dz$
$$A = 2\pi R\lambda + \frac{1}{2} R\epsilon^{2} k^{2} \lambda$$

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Physical interpretation

$$V = \int_0^\lambda dz \, \pi [R + \epsilon \cos(kz)]^2$$
$$\frac{V}{\lambda} = \pi R^2 + \frac{1}{2}\pi \epsilon^2$$
Require $V/\lambda = \pi R_0^2$, so $R = R_0 \left[1 - \frac{1}{2}\frac{\epsilon^2}{R_0^2}\right]^{1/2}$ To $O(\epsilon^2)$, $R = R_0 - \frac{1}{4}\frac{\epsilon^2}{R_0^2}$ Then, change in surface area of the jet (per unit wavel

Then, change in surface area of the jet (per unit wavelength) due to the displacement $R_{new} = R + \epsilon \cos(kz)$ is then

$$\frac{1}{2}\pi \frac{\epsilon^2}{R_0^2} [(2\pi R_0)^2 - \lambda^2)]$$

Physical interpretation

In terms of λ , the change in surface area is

$$\frac{1}{2}\pi \frac{\epsilon^2}{R_0^2 \lambda^2} [(2\pi R_0)^2 - \lambda^2]$$

For $\lambda > 2\pi R_0$, the surface area decreases.

Linear stability analysis: success stories



Critical Rayleigh number $Ra_c = 1708$. Experiments: 1705 ± 10 .

Linear stability analysis: success stories

Taylor-Couette Centrifugal Instability



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Stability of Parallel Shear Flows



- Parallel Base Flow: $\mathbf{U} = (U(y), 0, 0)$
- Perturbations: *u*, *v*, *w*

$$\begin{aligned} \frac{\partial u}{\partial t} + U \frac{\partial u}{\partial x} + vU' &= -\frac{\partial p}{\partial x} + \frac{1}{Re} \nabla^2 u \\ \frac{\partial v}{\partial t} + U \frac{\partial v}{\partial x} &= -\frac{\partial p}{\partial y} + \frac{1}{Re} \nabla^2 v \\ \frac{\partial w}{\partial t} + U \frac{\partial w}{\partial x} &= -\frac{\partial p}{\partial z} + \frac{1}{Re} \nabla^2 w \\ \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} &= 0 \end{aligned}$$

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Stability of Parallel Shear Flows

$$\nabla^2 p = -2U'\frac{v}{x}$$
• $\left[\left(\frac{\partial}{\partial t} + U\frac{\partial}{\partial x}\right)\nabla^2 - U''\frac{\partial}{\partial x} - \frac{1}{Re}\nabla^4\right]v = 0$
• $\left[\frac{\partial}{\partial t} + U\frac{\partial}{\partial x} - \frac{1}{Re}\nabla^2\right]\eta = -U''\frac{\partial v}{\partial z}$

- Normal vorticity: $\eta = \frac{\partial u}{\partial z} \frac{\partial w}{\partial x}$.
- Boundary conditions: $v = v' = \eta = 0$ at solid walls and in the far field.

Orr-Sommerfeld and Squire equations

•
$$v(x, y, z, t) = \tilde{v}(y) \exp[i(\alpha x + \beta z - \omega t)]$$

• $\eta(x, y, z, t) = \tilde{\eta}(y) \exp[i(\alpha x + \beta z - \omega t)]$
• $k^2 = (\alpha^2 + \beta^2)$

$$\begin{bmatrix} (-i\omega + i\alpha U)(\mathcal{D} - k^2) - i\alpha U'' - \frac{1}{Re}(\mathcal{D}^2 - k^2)^2 \end{bmatrix} \tilde{v} = 0$$
$$\begin{bmatrix} (-i\omega + i\alpha U) - \frac{1}{Re}(\mathcal{D}^2 - k^2) \end{bmatrix} \eta = -i\beta U'\tilde{v}$$

• BCs: $\tilde{v} = D\tilde{v} = \tilde{\eta} = 0$ at solid walls and in free stream.

Orr-Sommerfeld and Squire equations

- Temporal problem: α , β real, ω complex.
- Spatial problem: ω real, α , β complex.
- We will consider the temporal problem: c = ω/α is the complex wavespeed (eigenvalue) of the OS equation, and the associated v are the eigenfunctions.
- OS equation is homogeneous, while the Squire equation is forced by the solutions of the OS equation.
- Two classes of eigenmodes: OS modes and Squire modes.
- OS modes: Find ν_n and ω_n by solving OS equation and then find η_n^p by solving the inhomogeneous Squire equation.
- Squire modes: $\tilde{v} = 0$, $\tilde{\eta}_m \omega_m$

Squire's transformation and Squire's theorem

•
$$(U-c)(\mathcal{D}-k^2)\tilde{v}-U''\tilde{v}-\frac{1}{\mathrm{i}\alpha Re}(\mathcal{D}^2-k^2)^2\tilde{v}=0$$

- OS equation with $\beta = 0$ (no variation in the *z* direction): $(U-c)(\mathcal{D} - \alpha_{2D}^2)\tilde{v} - U''\tilde{v} - \frac{1}{i\alpha_{2D}Re_{2D}}(\mathcal{D}^2 - \alpha_{2D}^2)^2\tilde{v} = 0$
- Comparing: the two equations will have identical solutions if the following relations hold: α_{2D} = k = √α² + β²
 α_{2D}Re_{2D} = αRe
 ⇒ Re_{2D} = Re^α/_k < Re
- To each 3D OS mode, there is a corresponding 2D OS mode at a *lower* Reynolds number.

Squire's transformation and Squire's theorem

- Damped Squire modes: The solutions to the Squire equation are always damped with $c_i < 0$ for all α , β , and Re.
- To prove, multiply Squire equation by $\tilde{\eta}^*$ and integrate from y = -1 to y = 1 (the fluid domain), and take imaginary part.

$$c_i \int_{-1}^1 dy \, |\tilde{\eta}|^2 = -rac{1}{lpha Re} \int_{-1}^1 dy \, |\mathcal{D}\tilde{\eta}|^2 + k^2 |\tilde{\eta}|^2 < 0$$

Squire's theorem

Given Re_L as the critical Reynolds number for the onset of linear instability for a given α , β , the Reynolds number Re_c below which no exponential instabilities exisit for any wavenumber satisfies $Re_c \equiv \min_{\alpha,\beta} Re_L(\alpha,\beta) = \min_{\alpha} Re_L(\alpha,0)$

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Inviscid Analysis

Rayleigh Equation: Neglect viscous terms in OS equation

$$(U-c)(\mathcal{D}^2-k^2)\tilde{v}-U''\tilde{v}=0$$

with $k^2 = \alpha^2 + \beta^2$, and BCs: $\tilde{v} = 0$ at $y = \pm 1$ at solid boundaries.

- We have to forgo the no-slip BC due to the reduced order of the ODE.
- Since the coefficients of the Rayleigh equation are real, any complex eigenvalue will appear in conjugate pairs. If *c* is an eigenvalue, so is *c*^{*}.
- Regular singular point in the complex y plane when U(y) = c. The corresponding real part of this location y_c is the "critical layer" where U(y) = c_r.

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Inviscid Analysis

• Singularity is logarithmic, and Frobenius series can be used to find the solution about *y_c*.

$$\widetilde{v}_1(y) = (y - y_c)P_1(y)$$

 $\widetilde{v}_2(y) = P_2(y) + \frac{U_c''}{U_c'}\ln(y - y_c)$

Here, P_1 and P_2 are analytic.

- The second solution is multivalued due to the logarithmic term. When $c_i = 0$, the critical layer is on the real axis, $\ln(y - y_c) = \ln |y - y_c| \pm i\pi$ for $y < y_c$.
- The correct sign of the imaginary part cannot be determined within the inviscid analysis.
- Must do a matched asymptotic expansion of the Rayleigh invisicd solution with the full OS solution about $y = y_c$.

• Multiply Rayleigh equation by \tilde{v}^* and integrate from y = -1 to y = 1. Then integrate by parts:

$$\int_{-1}^{1} dy \, |\mathcal{D}\tilde{v}|^2 + k^2 |\tilde{v}|^2 + \int_{-1}^{1} dy \, \frac{U''}{U-c} |\tilde{v}|^2 = 0$$

• Take imaginary part:

$$c_i \int_{-1}^1 dy \ U'' \frac{|\tilde{v}|^2}{|U-c|^2} = 0$$

- Both $|\tilde{v}|^2$ and $|U c|^2$ are nonnegative. If c_i is positive, then U'' has to change sign in order for the integral to be zero.
- Rayliegh's inflexion point theorem only a necessary condition.

Rayleigh's inflexion point theorem

If there exist perturbations with $c_i > 0$, then U''(y) must vanish for some $y \in [-1, 1]$ for instability.

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$$\int_{-1}^{1} dy \, |\mathcal{D}\tilde{v}|^2 + k^2 |\tilde{v}|^2 + \int_{-1}^{1} dy \, \frac{U''}{U-c} |\tilde{v}|^2 = 0$$

Take real part:

$$\int_{-1}^{1} dy \, \frac{U''(U-c_r)}{|U-c|^2} = -\int_{-1}^{1} dy \, |\mathcal{D}\tilde{v}|^2 + k^2 |\tilde{v}|^2$$

Then add the following expression to the left side of above equation:

$$(c_r - U_s) \int_{-1}^{1} dy \ U'' \frac{|\tilde{v}|^2}{|U - c|^2} = 0$$

The above expression is zero due to inflexion point theorem V. Shankar (ChE, IITK) Hydrodynamic Stability SADEAFFP-2014 50 / 63

$$\int_{-1}^{1} dy \, \frac{U''(U-Us)}{|U-c|^2} |\tilde{v}|^2 = -\int_{-1}^{1} dy \, |\mathcal{D}\tilde{v}|^2 + k^2 |\tilde{v}|^2$$

For the integral to be negative, $U''(U - U_s) < 0$ in the flow field.

Fjortoft's Criterion

Given a monotonic mean velocity profile U(y), a necessary condition for instability is that $U''(U - U_s) < 0$, with $U_s = U(y_s)$ as the mean velocity at the inflexion point, i.e., $U''(y_s) = 0$.



FIGURE 2.3. Demonstration of Fjørtoft's criterion as a necessary condition for instability in inviscid flow (a) unstable according to Fjørtoft, (b) stable according to Fjørtoft

Howard's semicircle theorem

The unstable eigenvalues of the Rayleigh equation satisfy

$$\left[\mathsf{c}_{\mathsf{r}} - rac{1}{2} (U_{\mathsf{max}} + U_{\mathsf{min}})
ight]^2 + \mathsf{c}_{i}^2 \leq \left[rac{1}{2} (U_{\mathsf{max}} - U_{\mathsf{min}})
ight]^2$$

- For $c_i \rightarrow 0^+$, $U_{min} < c_r < U_{max}$ for marginally stable modes.
- For plane-Poiseuille flow and many internal channel flows, U" does *not* vanish in the domain of the flow, and so these flows are *stable* in the inviscid limit to 2D infinitesimal perturbations.
- Unbounded jets and free shear layers are unstable in the inviscid limit.

Viscous instability



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Numerical Eigenspectrum



FIGURE 3.1 Orr-Sommerfeld spectrum of plane Poiseuille flow for Re = 10000 (a) wave numbers $\alpha = 1, \beta = 0$. (b) wave numbers $\alpha = 0, \beta = 1$

Numerical Eigenspectrum



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Comparison with experiments

- Plane-Poiseuille flow (numerical solution): $Re_c = 5722.2$
- Experiments: *Re_c* could be as low as 1000.
- Pipe-Poiseuille flow (asymptotic/numerical solution): $Re_c = \infty$
- Experiments: $Re_c \sim 2000$.
- Plane Couette flow (numerical solution): $Re_c = \infty$.
- Experiments: $Re_c \sim 360$.
- Can a unavoidable disturbance in an experiment be treated as "infinitesimal" ?
- Very careful experiments in pipe flow: Re for transition could be 10^5 .
- Still need to explain the usual value of $Re \sim 2000$.

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- A toy nonlinear ODE: $\frac{dx}{dt} = ax bx^3$
- Base-state: $x = x_{B1} = 0$, $x = x_{B2} = +\sqrt{a/b}$, $x_{B3} = -\sqrt{a/b}$ for a/b > 0.
- Stability: x = x_{B1} + x', dx'/dt = ax', x'(t) = A exp[at], Unstable for a > 0 and Stable for a < 0.
- Stability of x_{B2} and x_{B3} : $\frac{dx'}{dt} = ax' 3bx_B^2x'$, $x'(t) = A \exp[st]$, s = -2a.
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Supercritical and Subcritical Bifurcation



- Supercritical bifurcation for b > 0: Solutions x_{B2} and x_{B3} exist only for a > 0; for a < 0, x = 0 is the only solution.
- For a > 0 x = 0 becomes unstable and gives rise to two new stable solutions x_{B2} or x_{B3}. (Rayleigh-Benard convection).
- Subcritical bifurcation for b < 0: For b < 0, x_{B2} and x_{B3} exist only for a < 0.
- For a < 0, x_{B2} and x_{B3} are unstable.
- The x = 0 solution could become unstable even for a < 0 to a sufficiently large disturbance (Shear flow instabilities).

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Hydrodynamic Stability

Weakly nonlinear effects: Landau equation

- Linear theory: $\frac{1}{A}\frac{dA}{dt} = s_0 A \Rightarrow A(t) = A(0) \exp[s_0 t]$
- When $s_0 > 0 \Rightarrow$ Flow unstable: Only onset predicted.
- Exponential growth: Cannot neglect nonlinearities anymore.
- Nonlinearities can saturate exponential growth, or further accelerate exponential growth.

Weakly nonlinear theory:

Landau Equation: $\frac{1}{A}\frac{dA}{dt} = s_0 + s_1 A^2$;

 s_1 : Landau constant \rightarrow effect of nonlinearities.

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Supercritical Equilibrium



•
$$\frac{1}{A}\frac{dA}{dt} = \underbrace{s_0}_{+ve} - |s_1|A^2 \Rightarrow A_s^2 = s_0/|s_1|.$$

- A linearly unstable mode saturates to a new steady state.
- Rayleigh Bernard convection cells, Taylor vortices . . .

Subcritical Instability





Stable to Small disturbances



Unstable to finite disturbances

- $\frac{1}{A}\frac{dA}{dt} = -\underbrace{|s_0|}_{-ve} + s_1 A^2 \Rightarrow \text{Instability for } \Gamma < \Gamma_c \text{ if } A_{intial}^2 > |s_0|/s_1.$
- A linearly stable mode becomes unstable to finite amplitude disturbances.
- Plane Poiseuille flow in a rigid channel: 65% reduction in critical Re for $v'_x/V = 0.025$; Strongly subcritical.

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Subcritical Instability



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Hydrodynamic Stability

Transient or algebraic growth: A simple example

• Coupled ODEs:
$$\frac{dv}{dt} = -\frac{1}{Re}v$$
, $\frac{d\eta}{dt} = v - \frac{2}{Re}\eta$

• Solution: Exponential decay of v(t) and $\eta(t)$

$$v(t) = v_0 \exp[-t/Re]$$

$$\eta(t) = v_0 Re(\exp[-t/Re] - \exp[-2t/Re]) + \eta_0 \exp[-2t/Re]$$

• For small times, series expand:

$$Rev_0(\exp[-t/Re] - \exp[-2t/Re]) = v_0t - \frac{3v_0}{Re}t^2 + \cdots$$

- Growth ∝ t for small times t < O(Re), and exponential decay for long times.
- During this "transient growth" nonlinearities could become important and lead to instabilities.
- "Bypass transition".

Transient or algebraic growth: A simple example

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Non-modal (transient) growth

- In rigid tubes, pipe flow always (asymptotically) stable at any *Re* as per normal mode analysis.
- Plane-Poiseuille flow unstable at $Re_c = 5772$, but experiments show instability at $Re \approx 1200$.
- Underlying differential operators are non-normal, and eigenfunctions are non-orthogonal.
- Possibility of algebraic or transient growth at early times, which eventually decay as $t \to \infty$.

Schmid and Henningson, 2001

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Spatio-temporal analysis

• Response to impulse forcing at x = 0, t = 0.



•
$$I(x,\omega) = \int_F \frac{d\alpha}{2\pi} D(k,\omega)^{-1} \exp(i\alpha x)$$

• Absolute instability: Contour deformation in the *L*-domain until there is a pinching of branches in the *F*-domain.