

# **Airborne Altimetric LiDAR: Principle, Data collection, processing and Applications**

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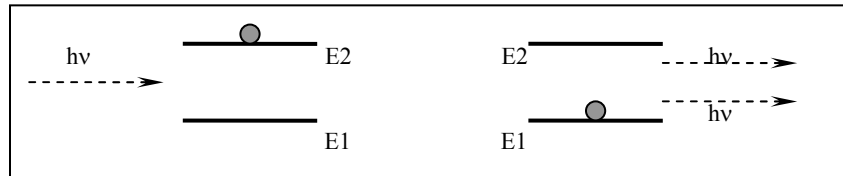
## **1 Introduction**

The recently emerged technique of airborne altimetric LiDAR (Light Detection and Ranging) provides accurate topographic data at high speed. This technology offers several advantages over the conventional methods of topographic data collection viz. higher density, higher accuracy, less time for data collection and processing, mostly automatic system, weather and light independence, minimum ground control required, and data being available in digital format right at beginning. Due to these characteristics, LiDAR is complementing conventional techniques in some applications while completely replacing them in several others. Various applications where LiDAR data are being used are flood hazard zoning, improved flood modeling, coastal erosion modeling and monitoring, bathymetry, geomorphology, glacier and avalanche studies, forest biomass mapping and forest DEM (Digital Elevation Model) generation, route/corridor mapping and monitoring, cellular network planning etc. The typical characteristics of LiDAR have also resulted in several applications which were not deemed feasible hitherto with the conventional techniques viz. mapping of transmission lines and adjoining corridor, change detection to assess damages ( e.g. in buildings) after a disaster.

This chapter aims at describing the various aspects of this technology, viz. physical principle, data collection issues, data processing and applications.

## 1.1 Laser

Laser (Light Amplification by the Stimulated Emission of Radiation) light is highly monochromatic, coherent, directional, and can be sharply focused.



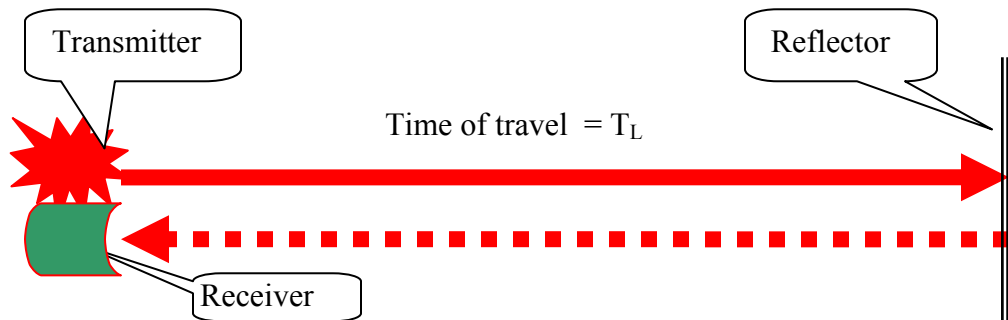
*Figure 1: Stimulated emission*

When a photon of energy  $h\nu$  ( $h$  is Planck's constant and  $\nu$  the frequency of radiation) interacts with an atomic system (Figure 1) which is in its upper state  $E_2$ , the system is driven down to its lower state  $E_1$  ( $h\nu = E_2 - E_1$ ) and two photons exit from the system. This process is called stimulated emission. The emitted photon is in every way identical with the triggering or stimulating photon. It has the same energy, direction, phase, and state of polarisation. Furthermore, each of these photons can cause another stimulated emission event and results in four photons emitted. Continuation of this process leads to a chain reaction. All photons emitted in this way have identical energies, directions, phases, and states of polarisation. This is how laser light acquires its characteristics.

The laser could be classified in many ways: pulsed and continuous; infrared, visible, and ultraviolet; high-power and low-power; and so on. The most important classification is into solid-state, gas, liquid, and semiconductor categories. For remote sensing purposes lasers capable of emitting high-power, short-duration, narrow-bandwidth pulse of radiant energy with a low degree of divergence are required. Lasers can be used for both spectral analysis and range measurement of a target. Altimetric LiDAR utilises the latter characteristic of the laser and discussions in the following sections will mostly concentrate on this. Therefore, the term LiDAR will, henceforth, generally mean range measurement or topographic LiDAR.

## 1.2 Principle of LiDAR

The principle of LiDAR is similar to Electronic Distance Measuring Instrument (EDMI), where a laser (pulse or continuous wave) is fired from a transmitter and the reflected energy is captured (Figure 2). Using the time of travel (ToT) of this laser the distance between the transmitter and reflector is determined. The reflector could be natural objects or an artificial reflector like prism. In case of ranging LiDAR this distance is one of the primary measurement which with integration with other measurements also provides the coordinates of the reflector. This is shown in the following paragraphs.

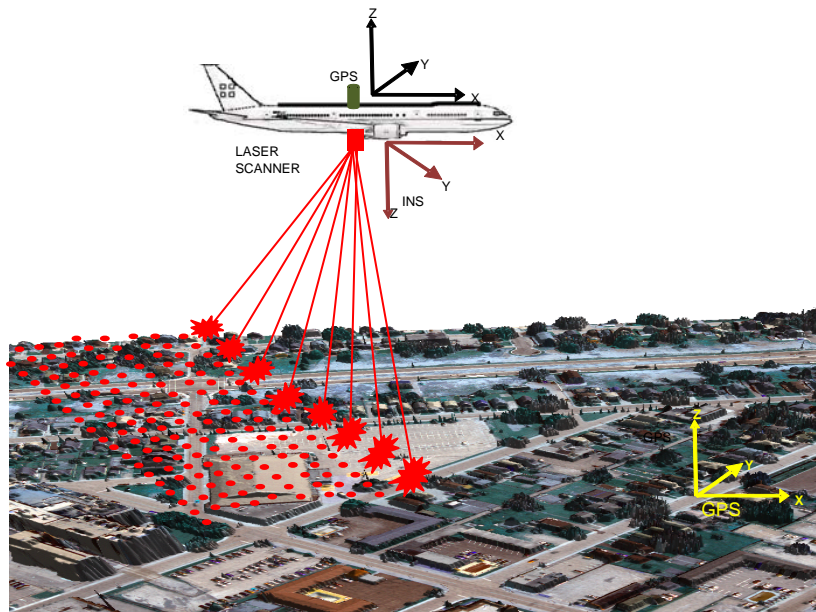


*Figure 2 Principle of range measurement using laser*

### 1.2.1 Topographic LiDAR

The Figure 3 shows the various sensors and scanning mechanism involved in LiDAR data collection. The basic concepts of airborne LiDAR mapping are simple. A pulsed laser is optically coupled to a beam director which scans the laser pulses over a swath of terrain, usually centred on, and co-linear with, the flight path of the aircraft in which the system is mounted, the scan direction being orthogonal to the flight path. The round trip travel times of the laser pulses from the aircraft to the ground are measured with a precise interval timer and the time intervals are converted into range measurements knowing the velocity of light. The position of the aircraft at the epoch of each measurement is determined by a phase difference kinematic GPS. Rotational positions of the beam director are combined with aircraft roll, pitch, and heading values determined with an inertial navigation system (INS), and with the range measurements, to obtain vectors

from the aircraft to the ground points. When these vectors are added to the aircraft locations they yield accurate coordinates of points on the surface of the terrain.



*Figure 3: Principle of topographic LiDAR*

The principle of using laser for range measurement was known since late 1960s. At the same time people began thinking about the use of airborne laser for measurement of ground coordinates. However, this could not be realized till late 1980s as determination of location of airborne laser sensor, which is a primary requirement, was not possible. The operationalization of GPS solved this problem. This is among the important reasons that why the laser mapping from airborne platform could not be realized before.

The LiDAR technology is known by several names in literature and industry. One may regularly come across the names like Laser altimetry, Laser range finder, Laser radar, Laser mapper and Airborne altimetric LiDAR. The term Airborne altimetric LiDAR (or Simply LiDAR) is the most accepted name for this technology.

The process of computation of ground coordinates is shown in the flow diagram ( Figure 4)

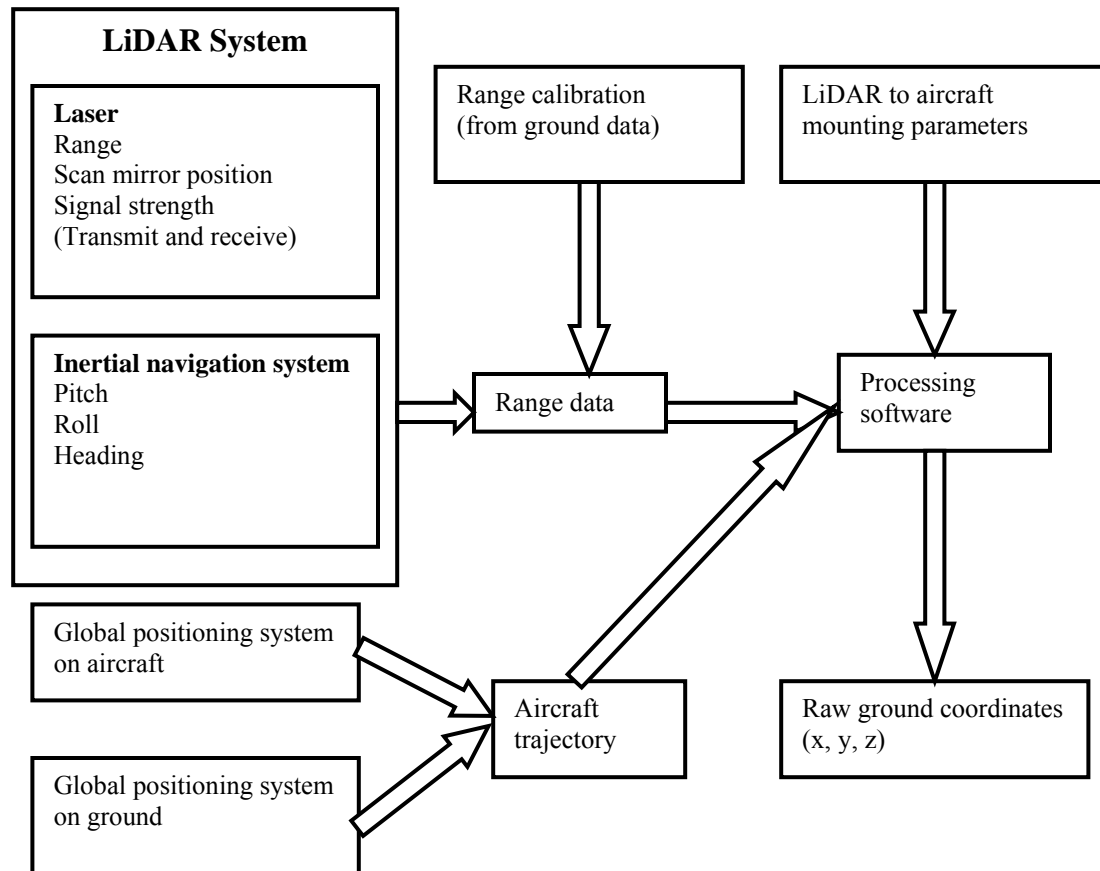
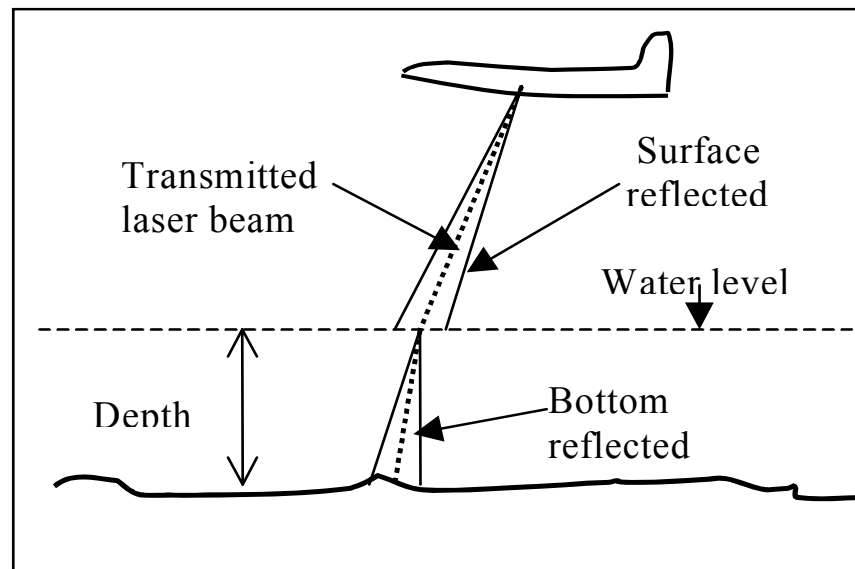


Figure 4: Flow diagram showing various sensors employed in LiDAR instrument and the computation steps

### 1.2.2 Bathymetric LiDAR

Most of the initial uses of LiDAR were for measuring water depth. Depending upon the clarity of the water LiDAR can measure depths from 0.9m to 40m with a vertical accuracy of  $\pm 15\text{cm}$  and horizontal accuracy of  $\pm 2.5\text{m}$ . As shown in Figure 5 a laser pulse is transmitted to the water surface where, through Fresnel reflection, a portion of the energy is returned to the airborne optical receiver, while the remainder of the pulse continues through the water column to the bottom and is subsequently reflected back to the receiver. The elapsed time between the received surface and bottom pulses allows determination of the water depth. The maximum depth penetration for a given laser system is obviously a function of water clarity and bottom reflection. Water turbidity plays the most significant role among those parameters. It has been noted that water

penetration is generally equal to two to three times the Secchi depth. Furthermore, the bottom and surface signals should be clearly distinctive to compute the water depth. In the case of shallow depths these signals overlap making it impossible to determine the water depth.



*Figure 5: Principle of Bathymetric LiDAR*

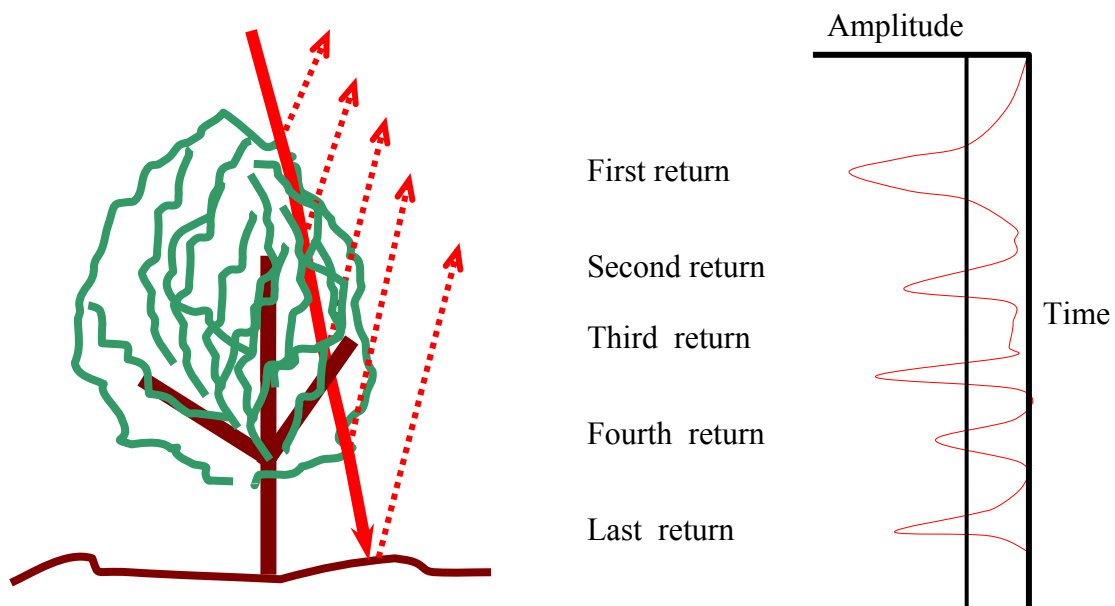
The wavelength used in this case is blue or green as these can transmit in the waterbody thus maximizing the measurable depth by LiDAR.

A hybrid LiDAR system employs both infra-red and green laser (concentric). While the infra red laser is reflected from land or from the water surface the green wavelength proceeds to and gets reflected from the bottom of water body. This makes it possible to capture both land topography and water bed bathymetry simultaneously.

### **1.2.3 Multiple return LiDAR**

A laser pulse has a finite diameter (~10 cm and larger). It is possible that only a part of the diameter comes across an object. This part of pulse will reflect from there, while the rest of the pulse keeps travelling till it encounters other objects which result in reflection of other parts of the pulse. On receiving the reflected laser pulse, the detector triggers

when the in-coming pulse reaches a set threshold, thus measuring the time-of-flight. The sampling of the received laser pulse can be carried out in different ways- sampling for the most significant return, sampling for the first and last significant return, or sampling all returns which are above threshold at different stages of the reflected laser waveform. Accordingly, the range is measured to each of those points wherefrom a return occurred to yield their coordinates.

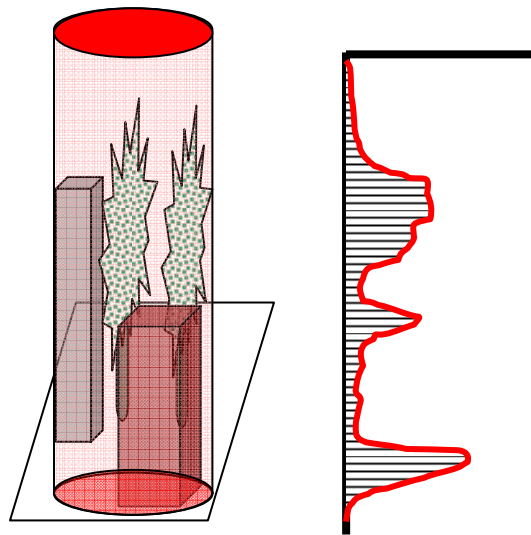


*Figure 6: Example of multiple returns from a tree*

In the figure shown above the first return is the most significant return. In case of capturing of only most significant return the coordinate of the corresponding point (here the top of tree) only will be computed. Capturing of first and last returns as shown above will result in determination of the height of the tree. It is important to note that last return will not always from the ground. In case of a laser pulse hitting a thick branch on its way to ground the pulse will not reach ground thus no last return from ground. The last return will be from the branch which reflected entire laser pulse. Commercially available sensors at present support up to 4 returns from each fired laser pulse and provide the option to choose among first, first and last and all 4 returns data.

### 1.2.4 Full waveform digitization

In this technique, the analogue echo signal is sampled at fine constant time intervals (black lines in Figure 7). The digital conversion of signal results in a digital data stream. The full wave measurement starts before the first detectable signal and lasts after the last detectable signal. The advantage of unlimited number of returns per pulse is that the canopy and sub-canopy details are revealed. The data can resolve surface roughness, slope and land cover within footprint. From full waveform the first significant return, first and last returns or multiple returns can be obtained in laboratory by data processing with more accuracy. The systems having this facility are RIEGL LMS-Q560, Litemapper and ALTM3100.



*Figure 7: Capture of full waveform by sampling the analogue waveform at close intervals.*

## 2 Physical principle of LiDAR

The following paragraphs discuss some of the basic concepts of LiDAR technology, which are important to understand technology and the data generated.



## 2.1 Types of range measurement

### 2.1.1 Continuous wave ranging

In this case a continuous beam of Electromagnetic Radiation (EMR) (light here) is used to measure the distance between transmitter and reflector. This is realized through the measurement of phase difference between transmitted and received wave. As shown in Figure 8, the time of travel can be written as:

$$T_L = nT + \frac{\phi}{2\pi}T$$

Where n is the total number of full wavelengths, T is time taken by light to travel equal to one wavelength and  $\phi$  is the phase difference. The only unknown in above is n which is determined using the techniques like decade modulation. So range is given by:

$$R = \frac{T_L}{2}c$$

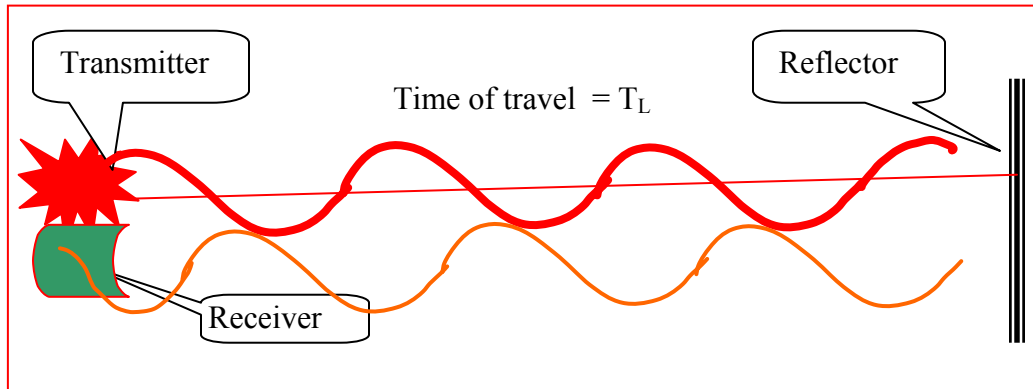


Figure 8 Continuous wave for phase difference measurement

For  $n = 0$

$$\text{Range } R = \frac{\phi}{4\pi}Tc = \frac{\phi}{4\pi} \frac{c}{f}$$

$$\text{so } \Delta R = \frac{c}{4\pi} \frac{\Delta\phi}{f}$$

The above shows that the range resolution depends upon the resolution of phase difference measurement and as well on the wavelength used. The advantage of CW measurement is that highly accurate measurements can be realised (as the accuracy of measurement is dependent upon the shortest wavelength used). However, it is difficult to generate continuous wave of high energy thus limiting the range of operation of these instruments. The slant range in case of airborne LiDAR is large thus the CW principle of ToT measurement is generally not used in these sensors.

The maximum range that can be measured by the CW LiDAR depends on the longest wavelength used, as shown below:

$$R_{\max} = \frac{\varphi_{\max}}{4\pi} \frac{c}{f} = \frac{2\pi}{4\pi} \lambda$$

$$\text{So } R_{\max} = \frac{\lambda_{\max}}{2}$$

### 2.1.2 Pulse ranging

As shown in Figure 9 the time of travel in pulse ranging is measured between the leading edges of transmitted and received pulse. The range measured is given by:

$$R = \frac{T_L}{2} c$$

Further, the range resolution and maximum range are given by:

$$\Delta R = \frac{c}{2} \Delta T_L \quad \text{and} \quad R_{\max} = \frac{c}{2} T_{L\max}$$

In case of pulse ranging the resolution of range measurement depends only on the resolution of ToT measurement, which is limited by the precision of the clock on the sensor. The maximum range that can be measured in pulse ranging depends upon the

maximum time that can be measured, as shown above. However, in practice the maximum range that can be measured depends upon energy of the laser pulse. The received signal should be of sufficient strength to be distinguished from the noise for detection. This in turn depends upon the divergence, atmosphere, reflectivity of target and detector sensitivity. In addition, the  $R_{max}$  also depends upon the pulse firing rate (PFR), i.e. number of pulses being fired in one second, which will be understood in later paragraphs.

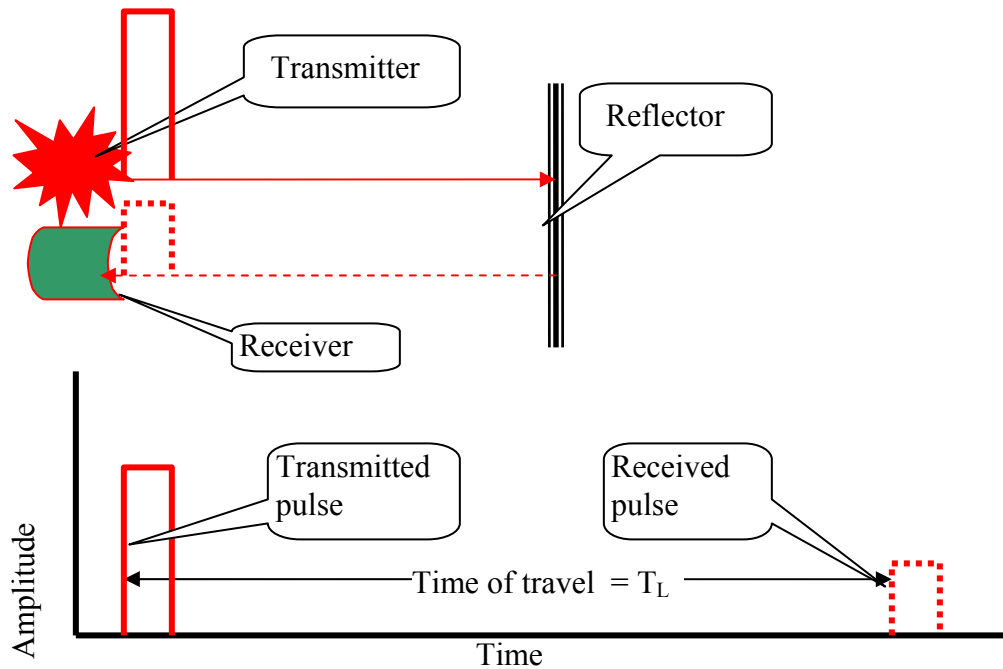


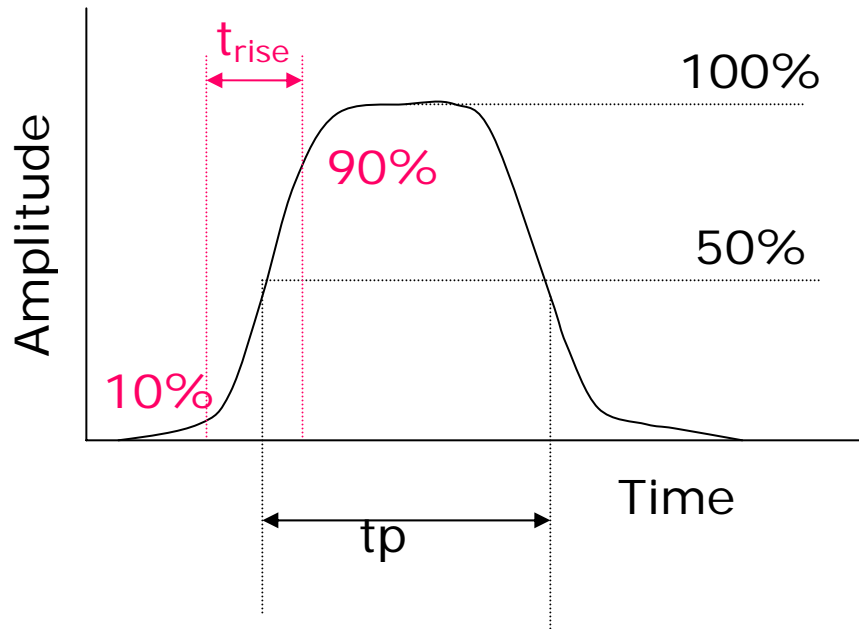
Figure 9: Time of travel measurement between transmitted and return pulse

It is clear from the above discussion that in airborne LiDAR pulse ranging is mostly employed. The discussion in rest of this document will thus be about pulse ranging only.

## 2.2 Laser pulse and nomenclature

Laser pulses are generated using the diode pumped solid state lasers, e.g. Ny-Yag laser. A typical laser pulse can be considered Gaussian in its amplitude distribution in both transverse and longitudinal directions. Figure 10 shows schematic of one such pulse. Here  $t_{rise}$  is the time taken by pulse to reach 90% amplitude from 10% amplitude. Pulse

width is defined as  $t_p$ , which is the duration between 50% amplitudes in leading and trailing edges of the pulse.



*Figure 10: A Gaussian pulse*

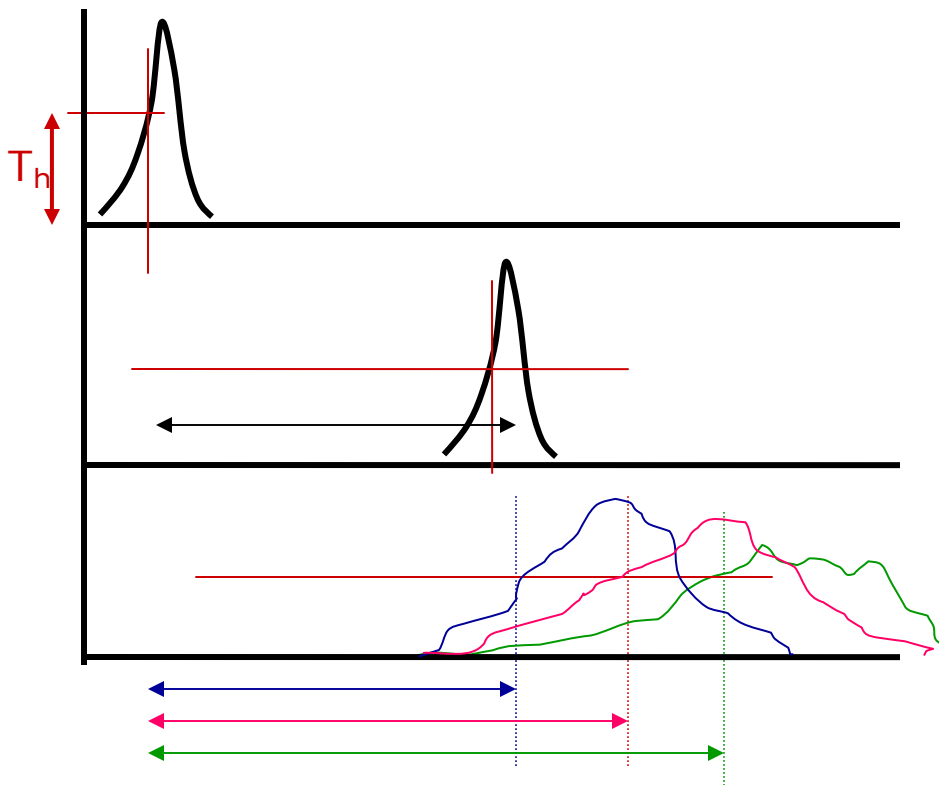
### **2.3 Time of Travel (ToT) measuring methods**

In the example of Figure 9 the transmitted and received pulse were assumed as the step pulses and ToT is measured with the well defined point on leading edges. However, in actual practice the transmitted pulse is Gaussian while the shape of return pulse depends upon the geometry, reflectivity and surface roughness with the laser footprint ( a laser footprint is the area on ground which is illuminated by the laser pulse, due to its divergence and a finite size of the transmission aperture) on ground. Therefore, it is quite common that the return pulse may have a distorted, multimodal and depleted shape. To measure the ToT on this one needs to define a point corresponding to a point on the transmitted pulse. The following methods are used for this purpose.

#### **2.3.1 Constant fraction method**

The ToT is measured w.r.t. a specific point on leading edge. The time counter is started by transmit pulse. Time counter stops when the voltage reaches a pre-

specified value for received pulse. This is measured on more steep leading edge/rising slope. In case of ideal return there will be no error in ToT measurement. However, due to different amplitude returns (different slopes of leading edges of return pulses) from the targets with different reflectivity and topology different ToT will be measured notwithstanding the targets being at same distance from the sensor. This is called range walk. Figure 11 shows how the ToT is measured for an ideal return (middle line) and for returns from targets of different reflectivity. The ToT measured for ideal return is without error, however, the range walk is introduced for other returns (lower line).



*Figure 11: Time measurement by constant fraction*

The error due to range walk needs to be eliminated. Some approaches for this will be discussed in following paragraphs.

### 2.3.2 Centroids of pulses

The ToT is measured between the centroids of transmitted and received pulse, as shown in Figure 12. For pulses which are distorted this method will yield error in time measurement.

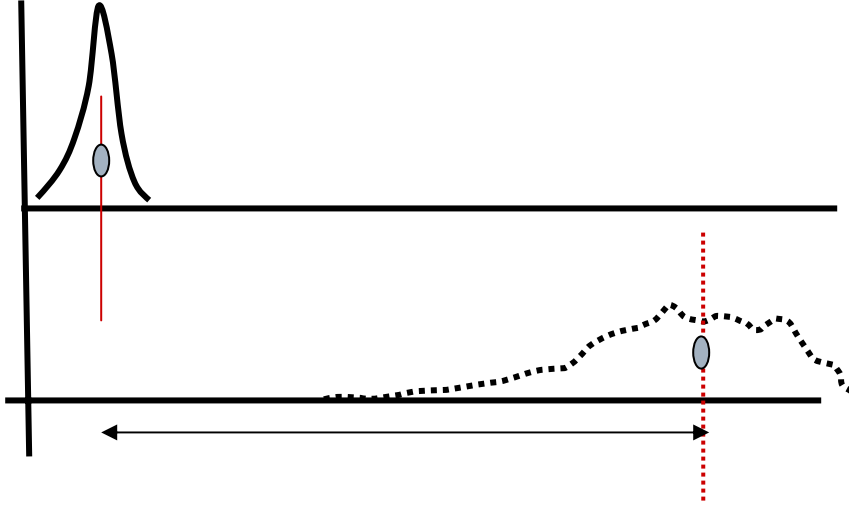


Figure 12: ToT measurement using centroids of the pulses

### 2.3.3 Correction using ratio of amplitudes

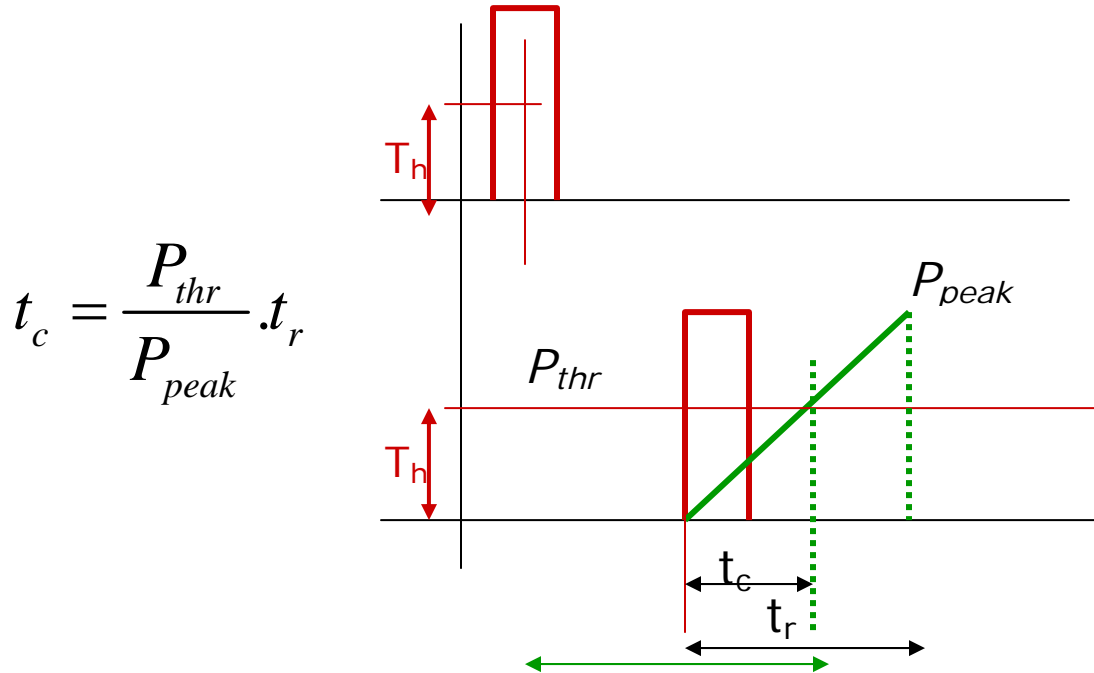
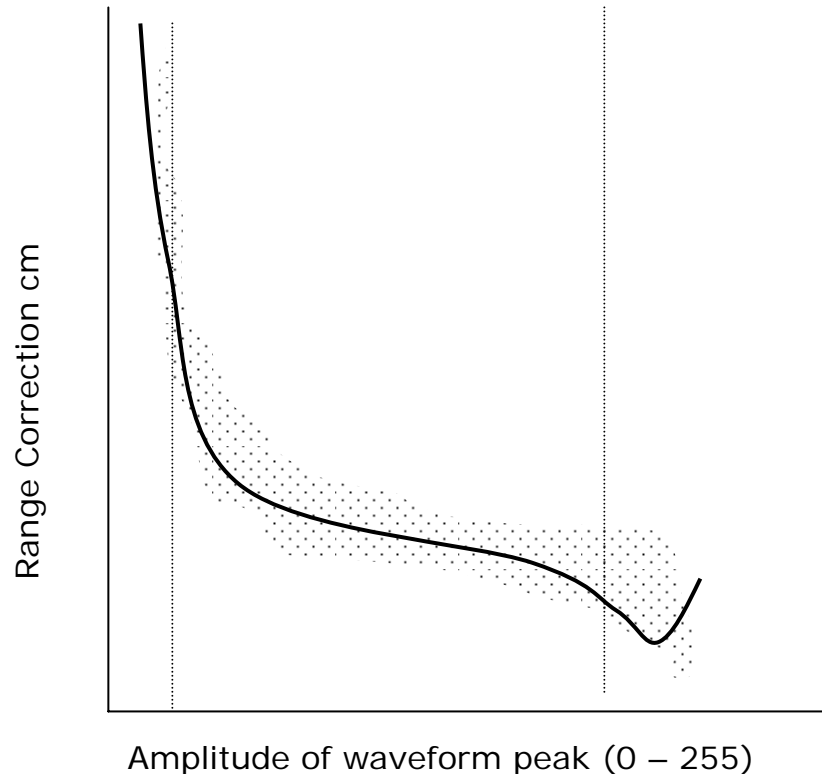


Figure 13: Correction to ToT using  $P_{peak}$

In this method correction to measured time is applied using the power of returned signal. The basic idea is to bring the time of travel to the level of step pulse, i.e., where for step pulse is being measured. The correction to be applied in measured time is given by  $t_c$  as shown in Figure 13:

#### 2.3.4 Correction using calibration



*Figure 14: Range calibration curve (Modified after Ridgway et al, 1997)*

This method aims at applying correction for range walk in range or in ToT measured by constant fraction method, as discussed above. The calibration data (time or range measured vs. amplitude of returned energy) are collected at a test site. The actual distance between sensor and target is known which is used to determine correction to time or range. The plot of correction versus amplitude of return pulse (as shown in Figure 14) is the calibration curve. The timings recorded by sensor are corrected by using the calibration curve for the measured values of return amplitude.

## **2.4 Requirement of the laser for altimetric LiDAR**

Altimetric LiDAR primarily uses the range measured by the laser ranger. To realise accurate and long range measurement the laser pulse should have the following characteristics:

- **High power:** So reflectance is available at receiver
- **Short pulse length:** Less uncertainty in time measurement
- **High collimation:** Less uncertainty due to smaller footprint
- **Narrow optical spectrum:** Small bandpass filter to reduce noise
- **Eye safety:** The lasers are more dangerous as wavelength reduces
- **Spectral reflectivity** of laser from terrain features: So reflectance (signal) is available.

## **2.5 LiDAR power and pulse firing rate**

For a pulse with  $P_{peak}$  power and  $t_p$  pulse width the energy in one pulse can be given by

$E = P_{peak} t_p$ . The total energy spent in one second will be  $P_{av} = EF$ , where  $F$  is the pulse firing rate (PFR). Thus the average power that is being spent per second is  $P_{av} = P_{peak} t_p F$ .

This leads to the conclusion that, for a given power and pulse width the PFR is inversely related to peak power of pulse. With the increase in altitude (range) one needs the pulses with higher peak power. For same value of  $P_{av}$  and  $t_p$ , thus with increase in altitude the PFR will reduce. This is reflected in the specifications of various sensors.

## **2.6 Geolocation of LiDAR footprint**

In LiDAR surveying the following basic measurements are obtained for each laser pulse fired:

- Laser range by measuring ToT of a pulse
- Laser scan angle
- Aircraft roll, pitch and yaw
- Aircraft acceleration in three directions



- GPS antenna coordinates

Geo-location means how to determine the coordinates of laser footprint in WGS-84 reference system by combining the aforesaid basic measurements.

As seen in Figure 15, a LiDAR system consists of three main sensors, viz. LiDAR scanner, INS and GPS. These systems operate at their respective frequencies. The laser range vector which is fired at a scan angle  $\eta$  in the reference frame of laser instrument will need to be finally transformed the earth centered WGS-84 system for realising the geolocation of the laser footprint. This transformation is carried through various rotations and transformations as shown below. First it is important to understand the various coordinate systems involved in this process and their relationships.

### 2.6.1 Reference systems

#### **Instrument Reference system:**

This is at centre of laser output mirror with Z axis along path of laser beam at centre of laser swath and X in the direction of aircraft nose while Y is as per right hand coordinate system. This is shown by black colour in Figure 15. This reference system will move and rotate with aircraft.

#### **Scanning reference system:**

The red lines in Figure 15 indicate the laser pulse and corresponding time-variable axis system with z being in the direction of laser pulse travel. The x axis is coincident with instrument reference X axis. The direction of z axis is fixed as per the instantaneous scan angle  $\eta$ .

#### **INS reference system (Body) :**

INS is aligned initially to local gravity and True North when switched on. It works by detecting rotation of earth and gravity. The origin of INS reference system is at INS with X, Y, Z defined as local roll, pitch, and yaw axes of airplane. Here X is along nose and Y along right wing of aircraft in a RH coordinate system. The INS gives the roll, pitch, and yaw values w.r.t. to the initially aligned system at any moment.

The above three reference systems are related to each other. Blue dotted lines are INS body axis with origin at instrument while black lines are instrument axis. These differ

due to mounting errors which are referred to as mounting biases in roll, pitch, and yaw and determined by calibration process. They also differ due to translation between INS and the laser head. The red lines indicate the laser pulse and corresponding time-variable axis system with  $z$  being in the direction of laser pulse travel. This is due to scan angle  $\eta$ . This reference system is related to instrument reference system with rotation angle  $\eta$ .

### **Earth tangential (ET) reference system**

It has its origin at onboard GPS antenna with  $X$  axis pointing in the direction of True north and  $Z$  axis pointing towards mass centre of Earth in a right handed system. This is variable for each shot in flight and can be conceptualized and realized computationally with the attitude measurements (Figure 16).

ET reference system is related to INS reference system by roll, pitch, and yaw measurements about  $X$ ,  $Y$ , and  $Z$ , respectively, at the time of each shot. ET is also related to Instrument System by the GPS vector measured in INS reference system. WGS-84 is related to ET by location of GPS antenna at the time of each laser shot.

### **2.6.2 Process for geolocation**

Range measurement is represented as a vector  $[0,0,z]$  in temporary scanning system. Rotate this vector in instrument reference system using scan angle ( $\eta$ ). Further rotate the vector in INS reference system with origin at instrument using the mounting angle biases ( $\alpha_0 \beta_0 \gamma_0$ ). Now this vector is translated by GPS vector  $[d_x, d_y, d_z]$  measured in INS reference system. Next step is to rotate the vector to the ET system using roll, pitch, yaw ( $\alpha \beta \gamma$ ). At this stage the vector is in ET system with origin at GPS antenna. Now rotate the vector in WGS-84 Cartesian system with origin at GPS antenna, using antenna latitude and longitude ( $\phi, \lambda$ ), which are measured by GPS. The vector is translated in Earth-centered WGS-84 system using Cartesian coordinates of antenna ( $a_x, a_y, a_z$ ), as observed by the GPS. The vector now refers to the Cartesian coordinates of laser footprint in WGS84, which can be converted in ellipsoidal system. If  $R_x(\theta)$  is rotation about  $x$  axis by  $\theta$  angle,  $T(V)$  is translation by a vector  $V$ ,  $[X']$  is final vector in WGS-84

system and  $\phi$  and  $\lambda$  are latitude and longitude of GPS antenna at the time of laser shot the aforesaid steps can be written as:

$$[x', y', z'] = [0, 0, z] R_x(\eta) R_x(\alpha_0) R_y(\beta_0) R_z(\gamma_0) T(d_x, d_y, d_z) R_x(\alpha) R_y(\beta) R_z(\gamma) R_y(\phi + \pi/2) R_z(-\lambda) T(a_x, a_y, a_z)$$

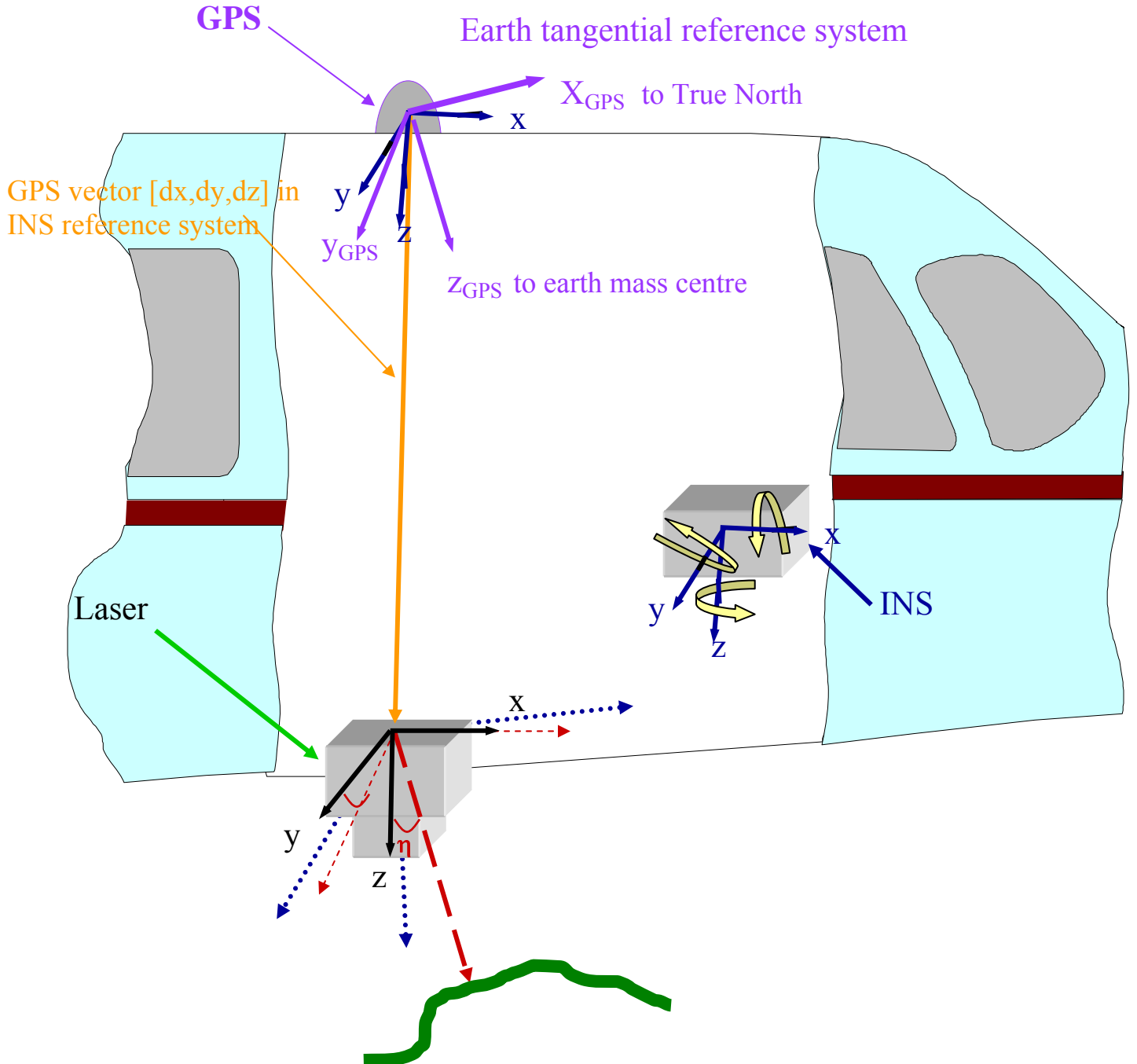


Figure 15: Relationship between laser scanner, INS and GPS and various reference systems.

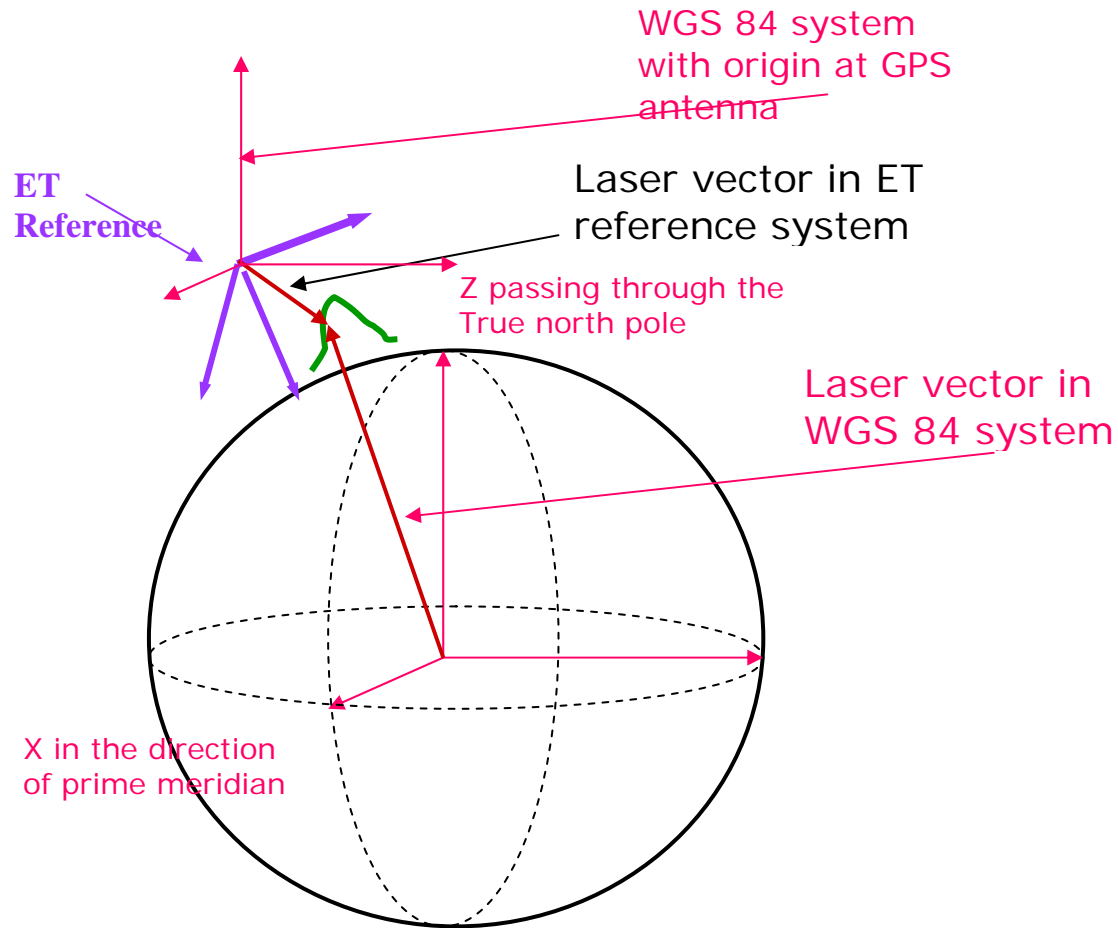


Figure 16: Relationship between ET and WGS-84 system

### 3 LiDAR sensor and data characteristics

#### 3.1 Available sensors

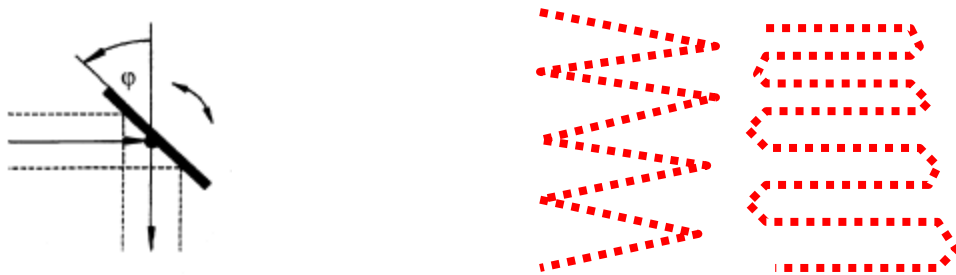
An excellent comparison of various available LiDAR sensors can be found at (Lemmens, 2007) . Sensors vary in their specifications and accordingly are suitable for collecting data with varied characteristics, as required in different applications. Moreover, each sensor possesses a large range of parameters in order to arrive at the required data specification. Some of the most commonly used sensors are ALTM by Optech Canada, ALS by Leica Geosystems, Toposys by Toposys GmbH, TopEye by Hansa Luftbild and RIEGL.

## 3.2 LiDAR Scanning pattern

Scanning pattern on ground depends primarily on the LiDAR sensors which scan the ground in different modes. The pattern also gets affected by the nature of terrain and the perturbations (attitude and acceleration) in flight trajectory. A few common types are described below:

### 3.2.1 Zig-zag pattern

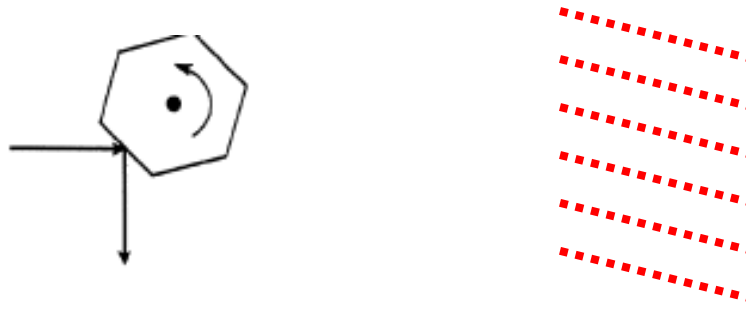
In this scanning (Figure 17) an oscillating mirror directs the laser pulse across the swath. With the use of galvanometers the pattern can be made more uniform. The data points are continuously generated in both directions of scan. The density of points is not uniform in these patterns, as points tend to come closure toward the end of swath due to deceleration of mirror. This problem is eliminated to some extent with the use of galvanometers. This is among the most common patterns and used in ALTM and Leica sensors.



*Figure 17: Zig-zag or meander type pattern*

### 3.2.2 Parallel line pattern

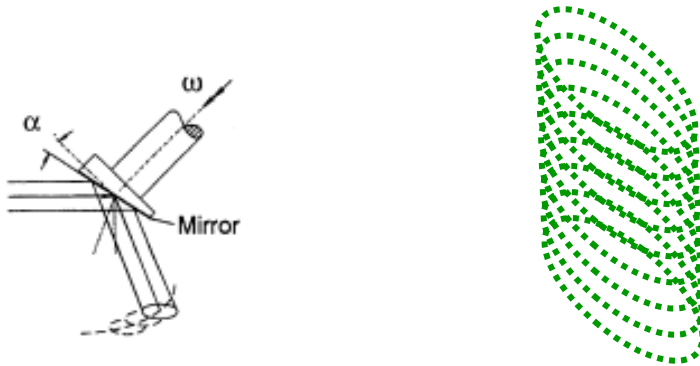
A rotating polygonal mirror directs the laser pulses along parallel lines across the swath. Data points are generated in one direction of scan only (Figure 18). The advantage of this is uniform spread of points on the ground.



*Figure 18: Parallel line pattern*

### 3.2.3 Elliptical pattern

As shown in Figure 19 the elliptical pattern is generated through a nutating mirror which rotates about its axis. The plane of mirror is at an inclination to rotation axis which causes the points to be fired in an elliptical pattern.



*Figure 19: Elliptical pattern*

### 3.2.4 Parallel lines-Toposys type

This pattern is typical to the Toposys sensors. Laser pulses are fired through an array of optical fibres and the return pulses are also collected through a similar system. The optical fibre array ensures that the scan lines are parallel and uniformly spaced on the ground as shown in Figure 20.

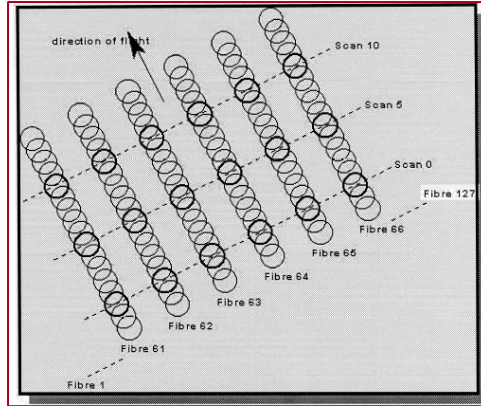


Figure 20: Parallel line pattern (Courtesy Toposys)

### 3.3 Data density

Data density is an important parameter in LiDAR survey. While a dense data captures the terrain better and helps in information extraction the time and resource requirement is high. The data density is decided depending the application for which the data are being collected. The data density mainly depends upon the parameters of sensor and platform e.g., flying height, velocity, scan angle, scan frequency, pulse firing rate, scanning pattern, acceleration and attitude variation of platform. Additionally, it also depends upon the ground geometry and reflectivity.

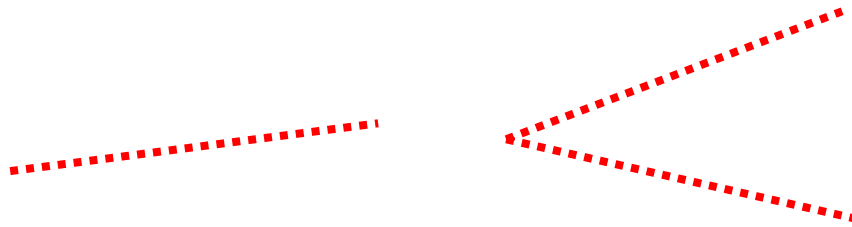


Figure 21: Scan definitions

Depending the sensor a scan could be of any of the two types as shown in Figure 21. Considering the scan frequency is  $f_{sc}$  the number of data points in one scan will be:

$$N = \frac{F}{f_{sc}}$$

If the platform is at an altitude of  $H$  and scan angle is  $\theta$  the swath  $S$  is given by:

$$S = 2H \tan\left(\frac{\theta}{2}\right)$$

Thus the data density (points per unit length) across the track (i.e. in the direction of scan) is given by :

$$d_s = \frac{N}{S} \text{ for unidirectional scan}$$

and

$$d_s = \frac{N}{2S} \text{ for bidirectional scan}$$

The data density along the track is variable for zig-zag scan and uniform for parallel line pattern. The maximum separation is given by:

$$d_{a\max} = \frac{v}{f}$$

Another approach to represent data density is as number of points in unit area. In this case the data density can be given by:

$$d = \frac{F}{vS}$$

where  $v$  is the velocity of airborne platform and  $vS$  is the area covered in one second while  $F$  is the number data points generated in one second. In above it is assumed all fired pulses will result in a measurement.

### 3.4 Example LiDAR data

An example LiDAR data is shown below for first and last return. LiDAR data are available either in ASCII format or in the standard .LAS format.

X	Y	Z	R	X	Y	Z	R
512548.36	5403119.37	314.29	10	512548.20	5403120.90	303.43	28
512548.39	5403120.61	313.73	20	512548.24	5403122.08	303.45	44
512548.36	5403122.39	308.73	48	512548.28	5403123.17	303.35	66
512548.40	5403123.05	310.07	26	512548.31	5403124.02	303.45	172
512548.40	5403123.92	308.46	0	512548.33	5403124.67	303.40	203
512548.34	5403125.09	303.43	290	512548.34	5403125.09	303.43	290
512548.35	5403125.41	303.47	319	512548.35	5403125.41	303.47	319
512548.35	5403125.74	303.47	319	512548.35	5403125.74	303.41	319
512548.36	5403125.95	303.46	290	512548.35	5403125.96	303.43	290

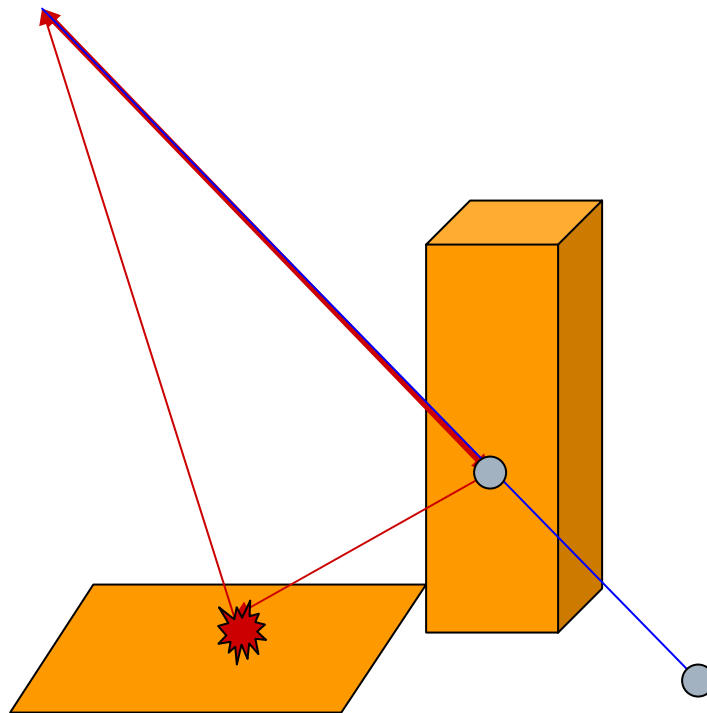


## 4 LiDAR error sources

The various sensor components fitted in the LiDAR instrument possess different precision. For example, in a typical sensor the range accuracy is 1-5 cm, the GPS accuracy 2-5 cm, scan angle measuring accuracy is  $0.01^\circ$ , INS accuracy for pitch/roll is  $< 0.005^\circ$  and for heading is  $< 0.008^\circ$  with the beam divergence being 0.25 to 5 mrad. However, the final vertical and horizontal accuracies that are achieved in the data are of order of 5 to 15 cm and 15-50 cm at one sigma. The final data accuracy is affected by several sources in the process of LiDAR data capture. A few important sources are listed below:

- Error due to sensor position due to error in GPS, INS and GPS-INS integration.
- Error due to angles of laser travel as the laser instrument is not perfectly aligned with the aircraft's roll, pitch and yaw axis. There may be differential shaking of laser scanner and INS. Further, the measurement of scanner angle may have error.
- The vector from GPS antenna to instrument in INS reference system is required in the geolocation process. This vector is observed physically and may have error in its observation. This could be variable from flight to flight and also within the beginning and end of the flight. This should be observed before and after the flight.
- There may be error in the laser range measured due to time measurement error, wrong atmospheric correction and ambiguities in target surface which results in range walk.
- Error is also introduced in LiDAR data due to complexity in object space, e.g., sloping surfaces leads to more uncertainty in X, Y and Z coordinates. Further, the accuracy of laser range varies with different types of terrain covers.
- The divergence of laser results in a finite diameter footprint instead of a single point on the ground thus leading to uncertainty in coordinates. For example, if sensor diameter  $D_s = 0.1$  cm; divergence = 0.25 mrad; and flying height 1000m, the size of footprint on the ground is  $D_i = 25$  cm. Varying reflective and geometric properties within footprint also lead to uncertainty in the coordinate.

- As shown in Figure 22, a laser may reflect in specular fashion from the wall of a building thus sending the pulse to some other than the instrument direction. Further, from the ground diffuse reflection takes place and a signal is captured at the sensor corresponding to this pulse. This will result in computation of a point which was never measured by the LiDAR, thus constitutes an outlier or an spurious data.



*Figure 22: Multipath in LiDAR results in spurious data points*

#### **4.1 Reporting LiDAR accuracy**

LiDAR accuracy is generally stated in vertical direction as the horizontal accuracy is indirectly controlled by the vertical accuracy. This is also due to the fact that determination of horizontal accuracy for LiDAR data is difficult due to the difficulty in locating Ground Control Points (GCPs) corresponding to the LiDAR coordinates.

The vertical accuracy is determined by comparing the Z coordinates of data with the truth elevations of a reference (which is generally a flat surface). The accuracy is stated as RMSE and given by:

$$RMSE_z = \sqrt{\frac{(\sum(Z_{data(i)} - Z_{check(i)})^2}{n}}$$

LiDAR accuracy is reported generally as 1.96 RMSE<sub>z</sub>. This accuracy is called fundamental vertical accuracy when the RMSE is determined for a flat, non-obtrusive and good reflecting surface. While the accuracy should also be stated for other types of surfaces, which are called supplemental and consolidated vertical accuracies.

## 5 Application of airborne altimetric LiDAR

Application areas for LiDAR can be divided in three main categories (1) Competing- where LiDAR is competing with existing topographic data collection methods; (2) Complementing- where LiDAR is complementing the existing topographic data collection methods and (3) New applications- where LiDAR data are finding applications in those areas which were not possible hitherto with the conventional data collection methods.

The following is a brief list of the areas where LiDAR data are being applied:

### 5.1 Floods

- Improving flood forecast models and flood hazard zoning operations with the use of more accurate topographic data.
- The information provided by LiDAR about the above ground objects can help in the determination of the friction coefficient on flood plains locally. This improves the performance of flood model.
- Topographic data input to GIS based relief, rescue, and flood simulation operations.

### 5.2 Coastal applications

- Coastal engineering works, flood management and erosion monitoring

- LiDAR is especially useful for coastal areas as these are generally inaccessible and featureless terrain. While being inaccessible prohibits land surveying or GPS survey the featureless terrain restricts use of photogrammetry due to absence of GCPs.
- The coastal landform mapping, e.g., mapping of tidal channels and other morphological features is possible by employing LiDAR data for change detection studies.

### **5.3 Bathymetric applications**

- For mapping river and coastal navigation channels and river and coastal bed topography

### **5.4 Glacier and Avalanche**

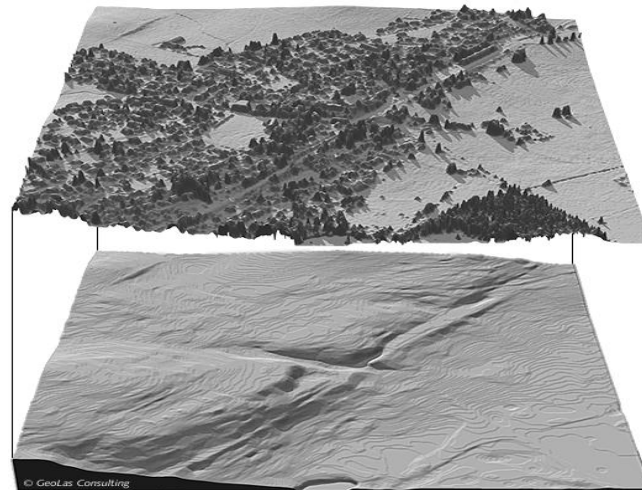
- Mapping glacial topography
- Attempts have been made for measuring ice velocities by comparing the relative position of glacial landforms on LiDAR data of two times.
- Risk assessment for avalanche by monitoring snow accumulation by LiDAR.

### **5.5 Landslides**

- Monitoring landslide prone zones. Continuous monitoring will lead to prediction of possible slope failures.

### **5.6 Forest mapping**

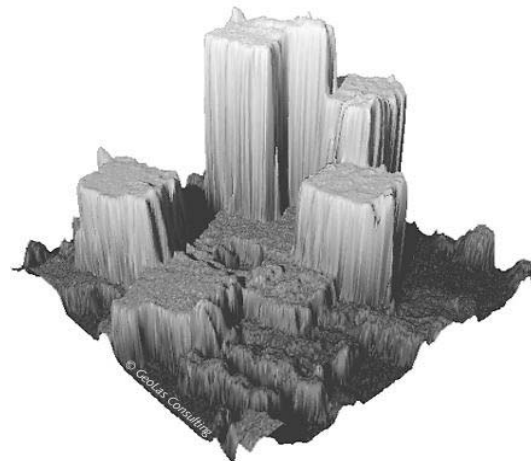
- LiDAR pulses are capable of passing through the small gaps in forest canopy. Thus data points will be available under the canopy of a tree. Algorithms are available which can separate the data points on trees and on the ground, thus producing a DEM of the forest floor (Figure 23). The forest floor DEM has applications in forest fire hazard zoning and disaster management
- As LiDAR data points are spread all over the canopy, models are being developed for estimation of biomass volume using LiDAR data.
- The information about percentage of points which penetrate the canopy of a tree can be related to the Leaf Area Index (LAI)



*Figure 23: LiDAR data of forest (top) and corresponding forest floor DEM (below)(Courtesy Geolas)*

## **5.7 Urban applications**

LiDAR data can be used for generating the maps of urban areas at large scale. LiDAR facilitates identification of buildings from the point cloud of data points, which are important for mapping, revenue estimation, and change detection studies. Drainage planning in urban areas needs accurate topographic data which are not possible to be generated in busy streets using conventional methods. The ability of LiDAR to collect data even in narrow and shadowy lanes in cities makes it ideal for this purpose. Accurate, dense and fast collection of topographic data can prove useful for variety of other GIS applications in urban areas, e.g. visualization, emergency route planning, etc.



*Figure 24: LiDAR data for a hotel (Courtesy Geolas)*

### **5.8 Cellular network planning**

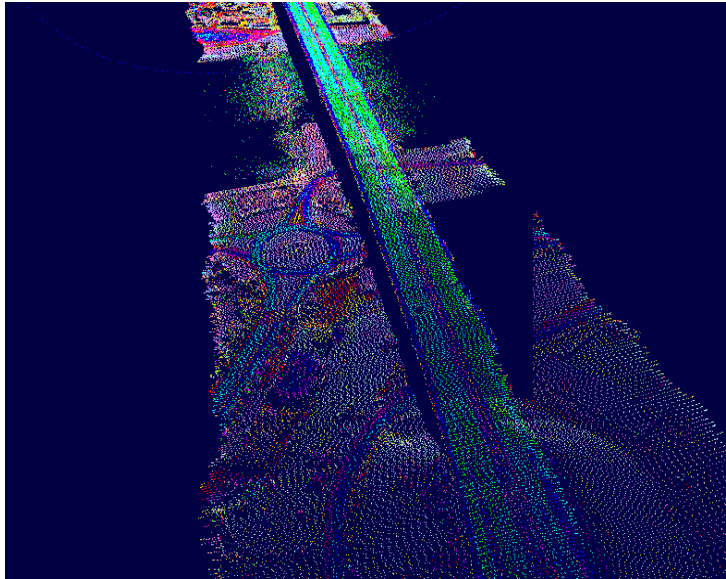
LiDAR collects details of building outlines, ground cover and other obstructions. This can be used to carry out accurate analysis for determining line of sight and view shed for proposed cellular antenna network with the purpose of raising an optimal network in terms of cost and coverage.

### **5.9 Mining**

- To estimate ore volumes
- Subsidence monitoring
- Planning mining operations

### **5.10 Corridor mapping**

This is among the most interesting applications of LiDAR data. A helicopter bound LiDAR sensor is generally used for mapping of corridor by flying at lower altitude for collecting accurate and dense data of corridors. A corridor may be highway, railway or oil and gas pipe line. The data are useful in planning the corridor and during execution of work and later for monitoring the deflections, possible areas of repair etc. High density of data facilitates generation of a record of the assets of the corridor.

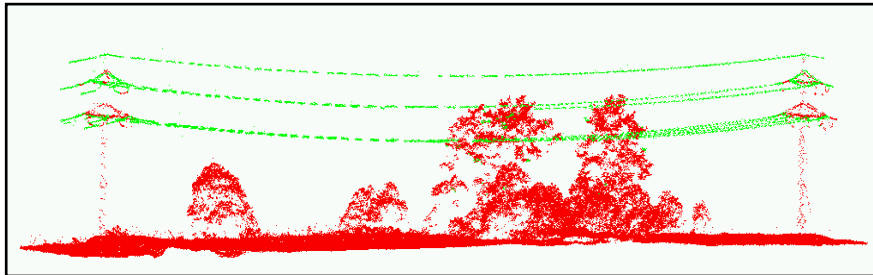


*Figure 25: A highway corridor captured using LiDAR data*

### **5.11 Transmission line mapping**

This is an area which was not possible with conventional topographic data techniques and where the LiDAR data are being used most. The LiDAR pulses get reflected highly from

the wires of transmission lines thus generating a coordinate at the wire. Multiple returns produce data for different story of wires. In addition, LiDAR also captures the natural and artificial objects under and around the transmission lines (Figure 26). This information is extremely useful for knowing tower locations, structural quality of towers, determining catenary models of lines, carrying out vegetative critical distance analysis and for carrying out repair and planning work in a transmission line corridor Figure 26.



*Figure 26: Transverse section of a transmission line using LiDAR data*

There are many more application areas for LiDAR data e.g., Creating realistic 3D environment for movies, games, and pilot training; Simulation of Hurricane movement and its effect; Simulation of Air pollution due to an accident or a polluting source; Transport of vehicular pollution in urban environment; etc. Basically, all those application areas where topographic data are fundamental can benefit with LiDAR data. LiDAR instruments are also being used for extra-terrestrial mapping (e.g. MOLA, LLRI)

## 6 Advantages of LiDAR technology

The other methods of topographic data collection are land surveying, GPS, inteferrometry, and photogrammetry. LiDAR technology has some advantages in comparison to these methods, which are being listed below:

- ❑ **Higher accuracy**

- Vertical accuracy 5-15 cm ( $1\sigma$ )
- Horizontal accuracy 30-50 cm

- ❑ **Fast acquisition and processing**

- Acquisition of 1000 km<sup>2</sup> in 12 hours.
- DEM generation of 1000 km<sup>2</sup> in 24 hours.

- ❑ **Minimum human dependence**
  - As most of the processes are automatic unlike photogrammetry, GPS or land surveying.
- ❑ **Weather/Light independence**
  - Data collection independent of sun inclination and at night and slightly bad weather.
- ❑ **Canopy penetration**
  - LiDAR pulses can reach beneath the canopy thus generating measurements of points there unlike photogrammetry.
- ❑ **Higher data density**
  - Up to 167,000 pulses per second. More than 24 points per m<sup>2</sup> can be measured.
  - Multiple returns to collect data in 3D.
- ❑ **GCP independence**
  - Only a few GCPs are needed to keep reference receiver for the purpose of DGPS. There is not need of GCPs otherwise.
  - This makes LiDAR ideal for mapping inaccessible and featureless areas.
- ❑ **Additional data**
  - LiDAR also observes the amplitude of back scatter energy thus recording a reflectance value for each data point. This data, though poor spectrally, can be used for classification, as at the wavelength used some features may be discriminated accurately.
- ❑ **Cost**
  - It has been found by comparative studies that LiDAR data is cheaper in many applications. This is particularly considering the speed, accuracy and density of data.

## **Reference:**

Lemmens, M., 2007, Airborne LiDAR Sensor: Product Survey, GIM International, 21(2)

Ridgway et al., 1997, Airborne laser altimeter survey of Long Valley California, Geophys. J. Int, 1331, 267-280